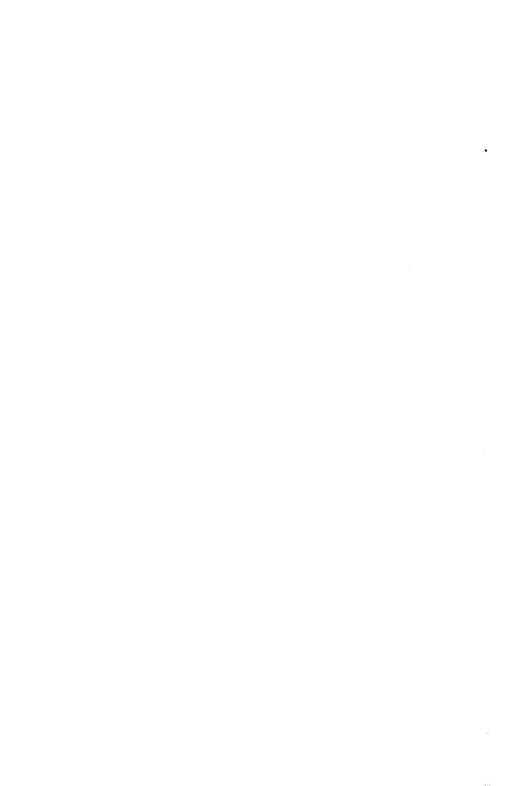
# 80 PRACTICAL TIME-SAVING PROGRAMS FOR THE TRS-80

DY CHARLES J. CARROLL

### 80 PRACTICAL TIME-SAVING PROGRAMS FOR THE TRS-80



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BY CHARLES J. CARROLL



FRASER VALLEY BEGIONAL LUBARI

### FIRST EDITION

### **FIRST PRINTING**

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### **Preface**



This book has one purpose: to be a time saver. In all the time spent writing and debugging programs, one of the most frustrating occurences is to need a formula for the particular program at hand. More times than not, precious time is spent looking for that elusive formula or its derivation. In this book I've tried to put in one single place many different types of programs with the hope that they will provide the necessary information you seek. Needless to say, many of the programs were direct results of my own interests. However, I've tried to add others from different fields to provide a suitable cross section.

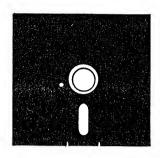
The biggest problem when writing this book was in hitting a happy medium between simple, mundane programs and more complicated, obscure ones. Ohms law, for instance, does not require a separate program. Its usage is wide enough that the formula should be at one's fingertips. In the same way that many of us have become dependent on the hand calculator (Quick: what's  $15 \times 12$ ?), myself included, we should not let the computer rule our existence down to the smallest detail. Remember, the calculator is an excellent time saver, not a crutch. Therefore, in this book you will see some basic indentity-type programs as well as some complicated single-purpose programs. Each, though, has been selected to provide a source of information. With this information at your finger tips, you, too, will hopefully, have more time for using your computer.

### **Dedication**

For My Very Organized Father From His Very Disorganized Son:

"Time has value, and we each spend that value for our own satisfactions."

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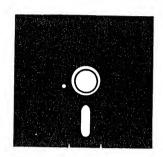
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### Chapter 1 Numbers



This chapter contains only seven different programs, but each program is useful in many different ways. The first three programs form the basis for many others, since complex operations and polar/rectangular conversions are used in many different facets of electronics. And, needless to say, where else do you find different bases but in computers?

I've tried to present the programs in such an order that the basic programs are first, followed by the more complex programs which may, or may not, use parts of the basic programs. In this way the later programs will be easier to understand, and you should be able to pull parts out as your own needs dictate.

### POLAR/RECTANGULAR CONVERSION

The polar/rectangular conversion is one of the most fundamental programs around. However, as with most of the other programs in this book, it's not one that you can recite without some extra time for thought. Figure 1-1 shows a diagram that relates the various components of the conversions.

To convert from polar to rectangular use the following equations:

$$X = M\cos T$$
  
 $Y = M\cos T$ 

where M is the magnitude and T is the angle in the polar notation. For rectangular to polar, use:

$$M = \sqrt{X^2 + Y^2}$$

$$T = \arctan(Y/X)$$

### Polar/Rectangular Conversion Program

- 5 'P/R CONVERSION
- 10 CLS
- 20 PRINT"SELECT APPROPRIATE FUNCTI ON P"CHR\$(94)"R(1) OR R"CHR\$ (94)"P(2)"
- 30 INPUT N
- 40 IF N=1 PRINT"ENTER MAGNITUDE, P HASE ANGLE": INPUT M,T ELSE GOTO 80
- 5Ø X=M\*COS(T\*, Ø1745329)
- 60 Y=M\*SIN(T\*.01745329)
- 70 PRINT"X="X" AND Y="Y:END
- 80 PRINT"ENTER X AND Y": INPUT X,Y
- 90 M=SQR(X+2+Y+2)
- 100 T=ATN(Y/X)\*57.29578
- 110 PRINT"MAGNITUDE="M "AND PHASE ANGLE="T

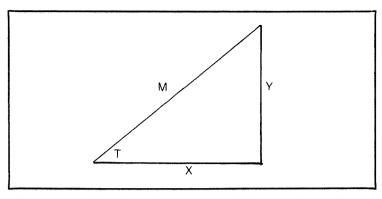


Fig. 1-1. How the various components of polar/rectangular conversions relate to each other.

### Sample Program

SELECT APPROPRIATE FUNCTION P ↑ R(1) OR R ↑ P(2)

?1

ENTER MAGNITUDE, PHASE ANGLE

?3,60

X = 1.5 AND Y = 2.59808

SELECT APPROPRIATE FUNCTION PAR (1) OR RAP (2)

?2

**ENTER X AND Y** 

? 5, 12

MAGNITUDE = 13 AND PHASE ANGLE = 67.3802

### **COMPLEX OPERATIONS**

The complex operations comprise the four basic arithmetic functions: addition, subtraction, multiplication and division of complex numbers. The equations for the functions are:

$$\begin{array}{l} {\rm addition} - ({\bf x_1} + i{\bf y_1}) + ({\bf x_2} + i{\bf y_2}) = ({\bf x_1} + {\bf x_2}) + ({\bf y_1} + {\bf y_2}) \ i \\ {\rm subtraction} - ({\bf x_1} + i{\bf y_1} + ({\bf x_2} + \iota{\bf y_2}) = ({\bf x_1} + {\bf x_2}) + ({\bf y_1} + {\bf y_2}) \iota \\ - ({\bf x_2} - ({\bf y_1} + \iota{\bf y_1}) \\ {\rm multiplication} - ({\bf x_1} + i{\bf y_1}) ({\bf x_2} + \iota{\bf y_2}) = {\bf M_1}/{\bf M_2} \ {\bf T_1} \\ {\rm division} - ({\bf x_1} + i{\bf y_1})/({\bf x_2} + i{\bf y_2}) = {\bf M_1}/{\bf M_2} \end{array}$$

where M and T are the respective magnitudes and phase angles from the rectangular to polar conversion.

### **Complex Operation Program**

```
5 'COMPLEX OPERATIONS
10 CLS
20 PRINT"SELECT THE APPROPRIATE CO
   MPLEX OPERATION"CHR$(13)TAB(20)
                       1"CHR$(13)TA
   "ADDITION
   B(20) "SUBTRACTION
                            2" CHR$ (
                                 3"
   13) TAB(20) "MULTIPLICATION
   CHR$(13)TAB(20)"DIVISION
      4"
30
    INPUT N
40 PRINT"ENTER FIRST COMPLEX NUMBE
   R (REAL, IMAGINARY)": INPUT FR, F
   T
50 PRINT"ENTER SECOND COMPLEX NUMB
   ER (REAL, IMAGINARY) ": INPUT SR,
   SI
60 IF N=1 GOTO 190
65 IF N=2 GOTO 170
70 FM=SQR(FR42+FI42)
8Ø FT=ATN(FI/FR)*57.29578
90 SM=SQR(SR42+SI42)
100 ST=ATN(SI/SR)*57.29578:IF N=3
    GOTO 150
110 AR=FM/SM
120 AI=FT-ST
130 BR=AR*COS(AI*.01745329)
140 BI=AR*SIN(AI*.01745329):GOTO 2
    10
```

150 AR=FM\*SM 160 AI=FT+ST:GOTO 130 170 BR=FR-SR 180 BI=FI-SI:GOTO 210 190 BR=FR+SR 200 BI=FI+SI:GOTO 210 210 PRINT"ANSWER (REAL, IMAGINARY) --- "BR;BI

### **Complex Operation Sample Program**

### SELECT THE APPROPRIATE COMPLEX OPERATION

ADDITION	1
SUBTRACTION	2
MULTIPLICATION	3
DIVISION	4

?3

ENTER FIRST COMPLEX NUMBER (REAL, IMAGINARY)

?3,5

ENTER SECOND COMPLEX NUMBER (REAL, IMAGINARY) ?6.-9

ANSWER (REAL, IMAGINARY)

--63 3.0

SELECT THE APPROPRIATE COMPLEX OPERATION

ADDITION	1
SUBTRACTION	2
MULTIPLICATION	3
DIVISION	4

?4

ENTER FIRST COMPLEX NUMBER (REAL, IMAGINARY)

? - 12, 3

ENTER SECOND COMPLEX NUMBER (REAL, IMAGINARY) ?4,-5

ANSWER (REAL, IMAGINARY)

-- 1.53658 1.17073

These two samples, multiplication and division, are the more difficult. They use the previous polar/rectangular conversion.

### **COMPLEX FUNCTIONS**

The four complex functions—absolute value, square, reciprocal, and square root—also use the polar/rectangular conversion. The respective formulas are:

absolute value - 
$$|x| = M$$
  
square -  $x^2 = M^2 / 2T$   
reciprocal -  $\frac{1}{x} = \frac{1}{M} / -T$   
square root  $\sqrt{x} = \pm (\sqrt{M} / T / 2)$ 

with M and T the magnitude and phase angle from the rectangular/polar conversion.

### **Complex Function Program**

5 'COMPLEX FUNCTIONS 10 CLS 20 PRINT"SELECT THE APPROPRIATE CO MPLEX OPERATION"CHR\$(13)TAB(20) "ABSOLUTE VALUE 1"CHR\$(13)TA B(20) "SQUARE 2" CHR\$ ( 13)TAB(20)"RECIPROCAL 3" CHR\$(13)TAB(20)"SQUARE ROOT 4" INPUT N 30 40 PRINT"ENTER COMPLEX NUMBER (REA L, IMAGINARY) ": INPUT R, I 50 M=SQR(R42+I42) 60 T=ATN(I/R)\*57.29578 70 IF N=1 PRINT"ANSWER -- "M:END E LSE IF N=2 GOTO 120 ELSE IF N=3 GOTO 100 80 AR=SQR(M)\*COS(T/2\*.01745329) 90 AI=SQR(M)\*SIN(T/2\*.01745329): GOTO 140 100 AR=1/M\*COS(-T\*.01745329) 110 AI=1/M\*SIN(-T\*.01745329):GOTO 140 120 AR=R42\*COS(2\*T\*.01745329) 130 AI=R42\*SIN(2\*T\*\*01745329):GOTO 140 140 PRINT"ANSWER (REAL, IMAGINARY) --"AR, AI

### **Complex Function Samples**

### SELECT THE APPROPRIATE COMPLEX FUNCTION

ABSOLUTE VALUE	1
SQUARE	2
RECIPROCAL	3
SQUARE ROOT	4

? 2 ENTER COMPLEX NUMBER (REAL, IMAGINARY) 2, -3 ANSWER (REAL, IMAGINARY) --- 5.0 - 12.0 SELECT THE APPROPRIATE COMPLEX FUNCTION

ABSOLUTE VALUE 1
SQUARE 2
RECIPROCAL 3
SQUARE ROOT 4

? 4 ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? –3. 5, 7 ANSWER (REAL, IMAGINARY) -- 2.37973 – 1.47076

### **CONVERSION TO BASE 10**

In this program, which converts a number to base 10, I've actually treated the number as a string and then operated on each integer individually. For example, the first of four digits is multiplied by the base to the third power (1234 $_3$  -- 1 × 3 $^3$ , 2 × 3 $^2$ , 3 × 3 $^1$ , and 4 × 3 $^0$  = 58). The basic equation is:  $N_{10} = X_n B^{n-1} + X_{n-1} B^{n-2} + X_{n-2} B^{n-3} \dots X_2 B + X$ 

### Conversion to Base 10 Program

- 5 'BASE CONVERSIONS
- 10 CLS
- 20 INPUT "ENTER NUMBER TO BE CONVE RTED TO BASE TEN"; X#
- 25 INPUT "ENTER BASE OF NUMBER TO BE CONVERTED"; B
- 30 N=LEN(STR\$(X#))-1
- 35 M=N-1
- 40 FOR @=2 TO N
- 50 S=S+VAL(MID\$(STR\$(X#),0,1))\*B\*M
- 55 M=M-1
- 60 NEXT Q
- 70 S=S+VAL(MID\$(STR\$(X#),0,1))
- 80 PRINTX#"BASE"B"EQUALS"S"BASE TE

### **Base 10 Conversion Samples**

ENTER NUMBER TO BE CONVERTED TO BASE TEN
? 3456
ENTER BASE OF NUMBER TO BE CONVERTED
? 7
3456 BASE 7 EQUALS 1266 BASE TEN
ENTER NUMBER TO BE CONVERTED TO BASE TEN
? 8776
ENTER BASE OF NUMBER TO BE CONVERTED
? 9
8776 BASE 9 EQUALS 6468 BASE TEN

### **CONVERSION FROM BASE 10**

As with the previous program, the conversion from base 10 to a new base is handled by treating the individual digits as part of a string. Each digit is separated from the string and operated on with the new base and its appropriate exponent. A FOR NEXT loop is used to evaluate the entire number. During the loop, the individual digits are again stored in a string until the completion of the process.

A number is changed to a new base by the following equation:

$$N_x = X - I_{n-1}B^{n-1} - I_{n-2}B^{n-2} \dots I_nB^n$$

### Conversion From Base 10 Program

```
5 'BASE CONVERSION
10 CLS
12 CLEAR 1000
15 P=1
25 DIM Z$(300)
30 INPUT "ENTER THE NUMBER TO BE C
   ONVERTED (BASE 10)";N
40 M=N
50 INPUT "ENTER NEW BASE" ; B
60 FOR I=0 TO 50
70 X=INT(B+I)
80 IF X>N GOTO 100
90 NEXT I
100 J=I
110 I=I-1
120 R=1
130 M=INT(M-INT(E+I))
140 IF M=0 Z$(P)=STR$(R): GOTO 220
145 IF M=INT(B+I)
                   GOTO 160
150 IF M<INT(B+I)
                   GOTO 180
160 R=R+1:GOTO 130
180 Z$(P)=STR$(R):PRINTZ$(P)
190 P=P+1
200 I=I-1
210 IF M>=INT(R+I) GOTO 120 ELSE R
    =Ø:GOTO 180
220 IF I=0 GOTO 250
230 FOR X=P+1 TO J
```

```
240 Z$(X)=STR$(A)

245 NEXT X

250 FOR Y=1 TO J

260 W$=W$+Z$(Y)

270 NEXT Y

280 PRINTN;"BASE 10 ="W$" BASE";B
```

### **New Base Conversion Samples**

```
ENTER THE NUMBER TO BE CONVERTED (BASE 10)
? 3112
ENTER NEW BASE
? 7
1
2
0
3
3112 BASE 10 = 12034 BASE 7
ENTER THE NUMBER TO BE CONVERTED (BASE 10)
? 1234
ENTER NEW BASE
? 2
1
0
0
1
1
0
1
0
1234 BASE 10 = 10011010010 BASE 2
```

### SIMULTANEOUS EQUATIONS

Use of this program will allow you to solve for two unknowns. Each of the unknowns is independently solved by using the coefficients of the terms in a matrix. Should the coefficients  $A \cdot E - B \cdot D = 0$ , the program will indicate a /  $\emptyset$  error. This indicates that either no solution or a unique solution exists. To solve for X and Y, the following equations are used:

$$X = \begin{vmatrix} C & B \\ E & D \\ \hline A & B \\ D & E \end{vmatrix} = \frac{CE - BF}{AE - BD} \quad Y = \begin{vmatrix} A & C \\ D & E \\ \hline A & B \\ D & E \end{vmatrix} = \frac{AF - DC}{AE - BD}$$

### Simultaneous Equations Programs

- 5 'SIMULTANEOUS EQUATIONS
- 10 CLS
- 20 PRINT"TO SOLVE SIMULTANEOUS EQU ATIONS FOR TWO UNKNOWNS, "CHR\$(1 3)"REARRANGE THE EQUATIONS INTO THE FOLLOWING FORMAT. "CHR\$(1 3)TAB(20)"AX+BY=C"CHR\$(13)TAB(2 0)"DX+EY=F"
- 30 INPUT"ENTER THE COEFFICIENTS -A,B,C,D,E,F";A,B,C,D,E,F
- 40 X=(C\*E-B\*F)/(A\*E-B\*D)
- 50 Y = (A\*F D\*C) / (A\*E B\*D)
- 60 PRINT"X="X"AND Y="Y

### Simultaneous Equations Examples

In the following examples, the program will be used to solve for X and Y in the two groups of equations:

$$2X + 3Y = -5$$
  
 $-5X - 2Y = 4$  and  $9.5X - 8.5Y = 3$   
 $2X + 4Y = -5$ 

TO SOLVE SIMULTANEOUS EQUATIONS FOR TWO UNKNOWNS.

REARRANGE THE EQUATIONS INTO THE FOLLOWING FORMAT.

$$AX + BY = C$$
  
 $DX + EY = F$ 

ENTER THE COEFFICIENTS -- A,B,C,D,E,F,

$$X = -.181818$$
 AND  $Y = -1.54545$ 

As proof:

$$2.-.181818 + 3.-1.54545 = -5$$
  
 $-5 \cdot -.181818 - 2 \cdot -1.54545 = 4$ 

For the second equation:

TO SOLVE SIMULTANEOUS EQUATIONS FOR TWO UNKNOWNS,

REARRANGE THE EQUATIONS INTO THE FOLLOWING FORMAT.

$$AX + BY = C$$
  
 $DX + EY = F$ 

ENTER THE COEFFICIENTS -- A,B,C,D,E,F,

$$X = -.554546$$
 AND  $Y = -.972727$ 

As proof: 
$$9.5 \cdot -.554546 - 8 \cdot -.972727 = 3$$
  
 $2 \cdot -.554546 + 4 \cdot -.972727 = -5$ 

### NUMERICAL INTEGRATION

This program for numerical integration provides an easy and convenient way to solve the common integral calculus problem. One especially useful case is to solve for the area under a curve. In fact, by solving for the area bounded by the curve which describes an antenna directivity pattern, the gain of that antenna can be calculated.

In this program you must use an odd number of points, and the points must be equally spaced. If data is not available for equally spaced points, try using one of the curve fitting programs to determine the equation of the line bounding the area. From this equation, equally spaced points can be selected and solved to provide data for the numerical integration.

The actual integration is solved by use of Simpson's Rule which is:

$$\int_{x^0}^{x_n} f(x) dx \cong \frac{S}{3}$$

$$[f(x_0) + 4f(x_1) + 2f(x_2) \dots 2f(x_{n-2}) + 4f(x_{n-1}) + f(x_n)]$$

### **Numerical Integration Program**

- 5 'NUMERICAL INTEGRATION
- 10 CLS
- 15 DIMV\$(100)
- 20 PRINT"ENTER THE SPACING BETWEEN THE SELECTED POINTS. AN ODD"CH R\$(13)"NUMBER OF POINTS MUST BE USED."
- 25 INPUT S:S=S/3
- 30 PRINT"ENTER THE VALUE FOR A SEL ECTED POINT. USE A / TO DENOTE "CHR\$(13)"THE END OF DATA."
- 40 FOR I=1 TO 100
- 50 INPUT V\$(I)
- 55 IF V\$(I)="/"GOTO80
- 60 V(I)=VAL(V\$(I))
- 65 0=0+1
- 70 NEXT I
- 80 NI=S\*V(1)+S\*V(0)
- 90 FOR I=2 TO Q-1STEP2
- 100 A=A+V(I)\*S\*4

- 110 NEXT I
- 120 FOR I=3 TO Q-2 STEP 2
- 130 B=B+V(I)\*S\*2
- 140 NEXT I
- 150 NI=NI+A+B
- 160 PRINT"ANSWER -- "NI

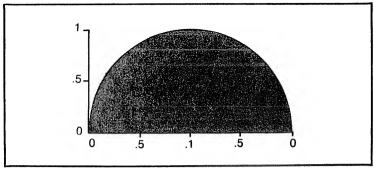


Fig. 1-2. The area (under the curve) which can be solved by using the 1st sample program for the numerical integration program.

### **Numerical Integration Sample Problems**

This first problem (see Fig. 1-2) will solve for the area under the indicated curve. The greater the number of points used, the more accurate the answer.

ENTER THE SPACING BETWEEN THE SELECTED POINTS. AN ODD NUMBER OF POINTS MUST BE USED.

? .314159

ENTER THE VALUE FOR A SELECTED POINT. USE A / TO DENOTE THE END OF DATA.

3.0

2.0955

? .3455

? .6545

? .9045

? 1,0000

? .9045

? .6545

? .3455

2.0955

? 0

? /

ANSWER -- 1.5708

If the program were set up for double precision, the actual answer would be 1.570794939994812. To see the difference in answer accuracy, the next example will be run using seven instead of eleven points.

ENTER THE SPACING BETWEEN THE SELECTED POINTS. AN ODD NUMBER OF POINTS MUST BE USED.

? .523598

ENTER THE VALUE FOR A SELECTED POINT. USE A / TO DENOTE THE END OF DATA.

9.0

? .25

? .6545

? 1

? .6545

? .25

2.0

ANSWER -- 1.5704

With double precision, the answer is 1.570412255525589. The actual difference in answers is very small, but it is used to illustrate that the number of points will influence the final answer.

And finally, since the area under the curve is really a semicircle, the actual answer is 1.570796327.



### Chapter 2 Finance

The following chapter focuses on financial programs and deals with three main areas: loans, savings, and compounded interest. In each case, we're generally concerned with what any payment might be, how much time or number of payments required, and total value.

The most basic programs deal with compounded amounts/interest. The main variables in the different equations are: initial deposit (A), interest rate (I), future value (V), number of years (T) and number of times the principal is compounded per year (TY). Equations for the following programs are:

$$\begin{split} V &= A \cdot (1 + I/TY) \phi(TY \cdot T) \\ T &= \log (\frac{V}{A}) / \log (1 + I/TY) \cdot TY \\ I &= \left( \left[ \frac{V}{A} \right] \right)^{\frac{1}{T \cdot TY}} - 1 \right) \cdot TY \end{split}$$

### **COMPOUND INTEREST**

This program will compute the final amount after some initial principal has been compounded periodically, with no further deposits. Additional deposit programs will be shown later in this chapter.

### **Compound Interest Program**

- 5 'COMPOUND INTEREST
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE COMPO-UNDED"; A
- 30 INPUT "ENTER INTEREST RATE"; I: I = I/100
- 40 INPUT "ENTER NUMBER OF YEARS MO NEY IS COMPOUNDED"; T
- 50 INPUT "ENTER NUMBER OF COMPOUND PERIODS PER YEAR": TY
- 62 V=A\*(1+I/TY) (TY\*T)
- 70 PRINT"\$"INT(V\*100+.5)/100

### **Sample Compound Interest Problems**

In these problems, the interest rate is entered as a percentage number rather than a decimal, i.e., 6 percent instead of 0.06. What will be the value of \$1500 in 9 years if it is deposited at 7.5 percent (year interest rate) and compounded quarterly?

ENTER AMOUNT TO BE COMPOUNDED? 1500

ENTER INTEREST RATE

? 7.5

ENTER NUMBER OF YEARS MONEY IS COMPOUNDED

?9

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

?4

\$2927.69

After \$15,000 is deposited for 20 years at 5.5 percent yearly interest (compounded semi-annually), what will be the total value of the principal?

ENTER AMOUNT TO BE COMPOUNDED

? \$15,000

**ENTER INTEREST RATE** 

? 5.5

ENTER NUMBER OF YEARS MONEY IS COMPOUNDED

? 20

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

?2

\$44,298

### YEARS OF INTEREST

This program deals with the number of years some principal will have to remain on deposit to reach a specific value.

### **Years of Interest Program**

- 5 'NO.YEARS OF COMPOUND INTEREST
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE COMPOUNDED"; A
- 30 INPUT "ENTER INTEREST RATE"; I: I = I/100
- 40 INPUT "ENTER FINAL DESIRED AMOUNT";V
- 50 INPUT "ENTER NUMBER OF COMPOUND PERIODS PER YEAR"; TY
- 60 T=LOG(V/A)/((LOG(1+I/TY))\*TY)
- 70 PRINT"COMPOUNDED"TY"TIMES PER Y EAR WILL REQUIRE THE MONEY TO B E DEPOSITED"INT(T\*10+.5)/10"YEA RS"

### Sample Problems

How many years will \$1000 dollars have to remain on deposit if the interest rate is 9.5 percent, the money is compounded quarterly, and the final desired amount is \$2000?

ENTER AMOUNT TO BE COMPOUNDED ? 1000

**ENTER INTEREST RATE** 

29.5

ENTER FINAL DESIRED AMOUNT

? 2000

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

?4

COMPOUNDED 4 TIMES PER YEAR WILL REQUIRE THE MONEY TO BE DEPOSITED 7.4 YEARS.

If the annual inflation rate averages 10 percent, in how many years will the price of some item double? For this problem assume that the price is currently \$100 and will double to \$200.

ENTER THE AMOUNT TO BE COMPOUNDED

? 100

**ENTER INTEREST RATE** 

? 10

ENTER FINAL DEPOSITED AMOUNT

? 200

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

?1

COMPOUNDED 1 TIME PER YEAR WILL REQUIRE THE MONEY TO BE DEPOSITED 7.3 YEARS.

Or, in other words, with an annual inflation rate of 10 percent, prices will double every 7.3 years!

### INTEREST RATE

With the many different types of savings instruments available, a person often has to evaluate each instrument versus his particular needs. This program is designed to calculate the amount of interest required to attain some final amount of money. This is especially useful with the varying amounts of time required by different savings plans. Note that the interest rate can also be considered as a rate of return for some initial deposit or investment.

### **Interest Rate Program**

- 5 'RATE OF RETURN
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE COMPO-UNDED"; A
- 30 INPUT "ENTER FINAL AMOUNT"; V
- 40 INPUT "ENTER NUMBER OF YEARS MO NEY IS COMPOUNDED";T
- 50 INPUT "ENTER NUMBER OF COMPOUND PERIODS PER YEAR"; TY
- 60 I = ((V/A) + (1/(TY\*T)) 1)\*TY
- 70 PRINT"RATE OF RETURN IS"I\*100"P ERCENT PER YEAR"

## Sample Interest Rate Problems

What interest rate is required to double your money in 2 years?

ENTER AMOUNT TO BE COMPOUNDED

?1

**ENTER FINAL AMOUNT** 

?2

ENTER NUMBER OF YEARS MONEY IS COMPOUNDED

22

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

?1

#### RATE OF RETURN IS 41.4214 PERCENT PER YEAR

Obviously, doubling your money requires a high rate of return, a rate that is not available through normal savings interest. Therefore, to double your money in a short period of time requires a more speculative type of investment, one that causes the chances of losing your money to increase in proportion to the rate of return.

You wish to make an initial deposit of \$5000 into a college education fund which will yield \$25000 in 15 years. If the money is compounded quarterly, what rate of return must the fund yield per year?

ENTER AMOUNT TO BE COMPOUNDED

25000

ENTER FINAL AMOUNT

? 25000

ENTER NUMBER OF YEARS MONEY IS COMPOUNDED

2 15

ENTER NUMBER OF COMPOUND PERIODS PER YEAR

24

RATE OF RETURN IS 10.8748 PERCENT PER YEAR

#### **FUTURE VALUE**

This group of programs deals with the same basic savings theme, though with periodic payments made into some savings instrument. First, the most basic: what is the future value of X dollars deposited Y times at Z interest? The equation for this computation is:

# **Future Value Program**

$$FV = \frac{A}{I} ((1+I)^{T+1} - (1+I))$$

- 5 'FUTURE VALUE
- 10 CLS
- 20 INPUT "ENTER AMOUNT OF MONTHLY DEPOSIT";A
- 30 INPUT "ENTER INTEREST RATE"; I:I = I/1200
- 40 INPUT "ENTER NUMBER OF YEARS";T :T=T\*12
- 5Ø FV=A/I\*((1+I) ↑ (T+1)-(1+I))
- 60 PRINT"\$"INT(FV\*100+.5)/100

# Sample Future Value Problems

How much money will a person have if he deposits \$200 each month for 10 years? The interest rate is 6 percent per year.

ENTER AMOUNT OF MONTHLY DEPOSIT

? 200

**ENTER INTEREST RATE** 

?6

ENTER NUMBER OF YEARS

? 10

\$32939.60

Note that the actual money deposited was \$24000 (\$2400/ year for 10 years).

#### REQUIRED PAYMENT

The next program deals with the required deposit each month to attain some specific goal. This is extremely useful when trying to determine how much money is available from a budget for the purchase of some article, i.e., a car payment. To determine the monthly payment, use the following equation:

$$A = \frac{FV \cdot I}{(1+I)^{T+1} - (1+I)}$$

## **Required Payment Program**

- 5 'PAYMENT FOR AMOUNT
- 10 CLS
- 20 INPUT "ENTER FINAL DESIRED AMOU NT"; FV
- 30 INPUT "ENTER INTEREST RATE"; I:I = I/1200
- 40 INPUT "ENTER NUMBER OF YEARS";T:T=T\*12
- 50 A=(FV\*I)/((1STEPRETURNSONLEFT\$

## **Sample Payment Problems**

You will need \$15000 in 7 years. How large a monthly payment do you need if the annual interest rate is 8.5 percent?

ENTER FINAL DESIRED AMOUNT

? 15000

**ENTER INTEREST RATE** 

28.5

ENTER NUMBER OF YEARS

?7

\$130.38 MONTHLY PAYMENTS

A new car costs \$7000. What is the monthly payment over 4 years if the interest rate is 12.5 percent? Disregard any interest payments.

ENTER FINAL DESIRED AMOUNT

? 7000

**ENTER INTEREST RATE** 

? 12.5

ENTER NUMBER OF YEARS

24

\$111.98 MONTHLY PAYMENTS

This amount is necessary to pay off the principal in 4 years. As you'll see later in this chapter, the amount required for interest payments raises the monthly payment considerably.

#### **NUMBER OF PAYMENTS I: SAVINGS**

The final program in this group of three (Future Value and Required Payment are the other two) will determine the number of equal payments necessary to achieve some final amount. As before, you will enter the monthly deposit, the total desired amount, and the interest rate.

To solve for the number of payments, use the following equation:

$$N = \frac{\frac{\log (V \cdot I}{A} + 1 + I)}{\log (1 + I)}$$

## **Number of Payments Program**

- 5 'NUMBER OF PAYMENTS
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE FINANC ED";P
- 30 INPUT "ENTER INTEREST RATE IN P ERCENT"; I:I=I/1200
- 40 INPUT "ENTER AMOUNT OF AFFORDAB LE MONTHLY PAYMENT"; A
- 50 N=LOG(A/(A-P\*I))/LOG(1+I)
- **60 PRINTN"MONTHLY PAYMENTS"**

# Sample Payments Program

How long will it take to save \$1200 if you are making monthly payments of \$15 at 10 percent interest?

ENTER AMOUNT OF MONTHLY PAYMENT

? 15

**ENTER INTEREST RATE** 

? 10

ENTER FINAL AMOUNT

? 1200

\$ 1200 WILL REQUIRE DEPOSITS OF \$15 FOR 61.1569 MONTHS

You make quarterly deposits of \$450 into a savings account. If the interest rate is 7.5 percent, how many months will it take to accumulate \$15000 in the account?

ENTER AMOUNT OF MONTHLY DEPOSIT

? 150 (450/3)

**ENTER INTEREST RATE** 

? 7.5

**ENTER FINAL AMOUNT** 

? 15000

\$15000 WILL REQUIRE DEPOSITS OF \$150 FOR 77.5398 MONTHS

(Or, quarterly deposits for 6.5 years)

# MONTHLY LOAN PAYMENT

This program will calculate the total monthly loan payment given the amount, interest rate, and number of payments. The program is based on:

$$A = P \left[ \frac{I/12}{1 - (1 - I/12)^{-N}} \right]$$

# **Loan Payment Program**

- 5 'MONTHLY LOAN PAYMENT
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE FINAN CED";P
- 30 INPUT "ENTER INTEREST RATE IN P ERCENT"; I: I = I/100
- 40 INPUT "ENTER NUMBER OF YEARS OF FINANCING"; N:N=N\*12
- 50 A=P\*(I/12)/(1-(1+(I/12))A-N)
- 60 PRINT"MONTHLY PAYMENT IS \$"INT( A\*100+.5)/100

# **Loan Payment Program Examples**

A new car costs \$7000. What is the monthly payment over 4 years if the interest rate is 12.5 percent?
ENTER AMOUNT TO BE FINANCED? 7000
ENTER INTEREST RATE IN PERCENT? 12.5
ENTER NUMBER OF YEARS OF FINANCING? 4
MONTHLY PAYMENT IS \$186.06

You'll note that this is considerably above the \$112 payment. Payment for the interest amounts to about two-thirds of the principal payment.

#### **LOAN BALANCE**

This section deals with the balance on a loan financed over some period of time. As demonstrated in the previous example (Monthly Loan Payment), payments on the interest are a significant portion of a monthly payment. In fact, in the case of a home mortgage, the interest payment is virtually the entire payment for the first several years. This Loan Payment program is designed to show the principal balance and accumulated interest after a desired number of payments. With this information, you can generate a schedule of interest paid, a number that is used when computing your Federal Income Tax return.

To compute the balance and interest, use:

$$B = \frac{1}{(1+I)^{-y}} \left[ A \cdot \frac{(1+I)^{-y}-1}{I} + P \right]$$

$$AI = B_y - B_{x-1} + (y-X+1) A$$

## Loan Balance Program

- 5 'LOAN BALANCE
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE FINAN CED";P
- 30 INPUT "ENTER INTEREST RATE IN P ERCENT"; I:I=I/1200
- 40 INPUT "ENTER MONTHLY PAYMENT"; A
- 50 INPUT "ENTER BEGINNING PAYMENT NUMBER"; X
- 60 INPUT "ENTER ENDING PAYMENT NUM BER"; Y
- 70 B=1/((I+1)↑-Y)\*((A\*(((1+I)↑-Y)-1))/I+P)
- 80 PRINT"BALANCE AT THE END OF PAY MENT NUMBER"Y"-- \$"INT(B\*100+.5)/100
- 90 AI=B-(1/((I+1))-(X-1))\*((A\*(((1 +I))-(X-1))-1))/I+P))+(Y-X+1)\*A
- 100 PRINT"ACCUMULATED INTEREST AT THE END OF PAYMENT NUMBER"Y"-- \$"INT(AI\*100+.5)/100

# Sample Loan Balance Problems

A \$40000 mortgage is arranged such that the first payment is in January. The mortgage is 9 percent over 30 years and the payment is \$321.85 (use the previous program for Monthly Loan Payment to compute the payment). Determine the interest paid after the first, fifth, twentieth, and thirtieth year.

ENTER AMOUNT TO BE FINANCED

?40000

ENTER INTEREST RATE IN PERCENT

29

ENTER MONTHLY PAYMENT

2.321.85

ENTER BEGINNING PAYMENT NUMBER

21

ENTER ENDING PAYMENT NUMBER

? 12 (12th month)

BALANCE AT THE END OF PAYMENT NUMBER 12 — \$39726.70

ACCUMULATED INTEREST AT THE END OF PAYMENT NUMBER 12 — \$3588.92

ENTER AMOUNT TO BE FINANCED

? 40000

ENTER INTEREST RATE IN PERCENT

29

ENTER MONTHLY PAYMENT

? 321.85

ENTER BEGINNING PAYMENT NUMBER

249

ENTER ENDING PAYMENT NUMBER

? 60

BALANCE AT THE END OF PAYMENT NUMBER 60 — \$38352 ACCUMULATED INTEREST AT THE END OF PAYMENT NUMBER 60 — \$3471.02

The total amount paid per year on the mortgage is \$3862.20. So even at the end of the fifth year, almost 90 percent of the monthly payment is still going for interest payments. However, look at the situation in the fifteenth and twentieth years:

ENTER AMOUNT TO BE FINANCED

? 40000

ENTER INTEREST RATE IN PERCENT

?9

**ENTER MONTHLY PAYMENT** 

? 321.85

ENTER BEGINNING PAYMENT NUMBER

? 169

ENTER ENDING PAYMENT NUMBER

? 180

BALANCE AT THE END OF PAYMENT NUMBER 180 — \$31732.10

ACCUMULATED INTEREST AT THE END OF PAYMENT NUMBER 180 — \$2903.31

ENTER AMOUNT TO BE FINANCED

?40000

ENTER INTEREST RATE IN PERCENT

?9

**ENTER MONTHLY PAYMENT** 

? 321.85

ENTER BEGINNING PAYMENT NUMBER

? 229

ENTER ENDING PAYMENT NUMBER

? 240

BALANCE AT THE END OF PAYMENT NUMBER 240 — \$25407.30

ACCUMULATED INTEREST AT THE END OF PAYMENT NUMBER 240 — \$2360.87

Even at the end of the twentieth year, more than 60 percent of the total payment is still going for interest.

#### NUMBER OF PAYMENTS II: LOAN

How long will it take to pay something off with a known monthly payment? This is not an unusual question in today's finances. To calculate the number of payments, use the following equation:

$$N = \frac{\log(1 - \frac{I \cdot A}{P})}{\log(1 + I)}$$

## **Number of Payments Program**

- 5 'NO. OF PAYMENTS
- 10 CLS
- 20 INPUT "ENTER AMOUNT OF MONTHLY DEPOSIT";A
- 30 INPUT "ENTER INTEREST RATE"; I: I =I/1200
- 40 INPUT "ENTER FINAL AMOUNT"; V
- 50 N = (LOG(V \* I/A + 1 + I) / (LOG(1 + I)) 1)
- 60 PRINT"\$"V"WILL REQUIRE DEPOSITS
  OF \$"A"FOR"N"MONTHS"

# **Number of Payments Examples**

If I can afford a monthly payment of \$150 and the prevailing interest rate is about 12 percent, how many payments will it take to pay off a loan of \$5000?

ENTER AMOUNT TO BE FINANCED
? 5000
ENTER INTEREST RATE IN PERCENT
? 12
ENTER AMOUNT OF AFFORDABLE MONTHLY PAYMENT
? 150
40.7 MONTHLY PAYMENTS

#### **LOAN AMOUNT**

Conversely, instead of how many months it will take to pay something off, let's try: "How much can I afford to spend if I commit so much per month to another payment?" The equation for this program is:

$$P = A \cdot \left(\frac{1 - (1 + I)^{-N}}{I}\right)$$

## **Loan Amount Programs**

- 5 'LOAN AMOUNT
- 10 CLS
- 20 INPUT"ENTER NUMBER OF PAYMENTS DESIRED" N
- 30 INPUT "ENTER INTEREST RATE IN P ERCENT"; I: I = I / 1200
- 40 INPUT "ENTER AMOUNT MONTHLY PAY MENT"; A
- 50 P = A \* (1 (1 + I) A N) / I
- 60 PRINT"YOU CAN AFFORD TO BORROW \$"P

# **Sample Loan Amount Programs**

If I can afford to pay \$100 per month for the next 15 months, how much new furniture can I purchase if the interest rate is 12 percent?

ENTER NUMBER OF PAYMENTS DESIRED

? 15

ENTER INTEREST RATE IN PERCENT

? 12

ENTER AMOUNT OF MONTHLY PAYMENT

? 100

YOU CAN AFFORD TO BORROW \$ 1386.49

Current car loans have an interest rate of 10.75 percent. If a new car loan runs for 4 years, how much can I afford if my monthly payment is \$ 150?

ENTER NUMBER OF PAYMENTS DESIRED

?48

ENTER INTEREST RATE IN PERCENT

? 10.75

ENTER AMOUNT OF MONTHLY PAYMENT

? 150

YOU CAN AFFORD TO BORROW \$5831.05

#### SINKING FUND

The last program in this chapter is for a sinking fund type of payment. The sinking fund method of payment is based on accumulating money through periodic deposits which also earn some interest. To calculate the monthly deposit use the formula:

$$A = \frac{P \cdot I}{(1+I)^N - 1}$$

## **Sinking Fund Program**

- 5 'SINKING FUND
- 10 CLS
- 20 INPUT "ENTER AMOUNT TO BE ACCUMULATED";P
- 30 INPUT "ENTER INTEREST RATE IN P ERCENT"; I:I=I/100
- 40 INPUT "ENTER NUMBER OF YEARS OF ACCUMULATION"; N
- $50 A=P*I/(((1+I)^{4}N)-1)$
- 60 PRINT"YEARLY DEPOSIT IS \$"INT( A\*100+.5)/100

# **Sinking Fund Examples**

How much money must be deposited at the end of each year in a 5-year sinking fund to accumulate \$5000 if the annual interest rate is 7.5 percent?

ENTER AMOUNT TO BE ACCUMULATED ? 5000
ENTER INTEREST RATE IN PERCENT ? 7.5
ENTER NUMBER OF YEARS OF ACCUMULATION ? 5
YEARLY DEPOSIT IS \$860.82



# Chapter 3 Statistics

This chapter on statistics will deal with several different areas, not just the common mean standard deviation. Included are programs on curve fitting, probability, and number evaluation. Some of the problems will find use within other even larger problems. And, as mentioned in Chapter 2, some of the programs can be used to supply data for other areas.

#### **PERMUTATIONS**

The first program in this chapter deals with the operation known as permutations. Or, how many different *ordered* groups can be obtained from some set of objects without repetition. As an example, how many 3-letter permutation groups are there in the letters W, X, Y, and Z?

To solve the permutation problem requires the use of the factorial operation. To explain, 3 factorial, represented as 3!, is the product of the form  $3 \cdot 2 \cdot 1 = 6$ . The 3 denotes the highest integer in the series. On the other hand, 5! would equal 120 ( $5 \cdot 4 \cdot 3 \cdot 2 \cdot 1 = 120$ ).

The general equation for a permutation is:

$$M^{P}N = \frac{M!}{(M-N)!}$$

Therefore, the previous question of how many 3-letter permutation groups are there in the letters W, X, Y, and Z could be expressed as  $4^P3$ .

Evaluating this expression produces  $4^{P}3 = \frac{4!}{(4-3)!} = \frac{4!}{1!} =$ 

$$\frac{4 \cdot 3 \cdot 2 \cdot 1}{1} = 24.$$

# **Permutation Program**

```
5 'PERMUTATIONS
10 CLS
20 PRINT"INPUT M":INPUT M
30 PRINT"INPUT N":INPUT N
40 IF N=0 P=1:GOTO 110
50 IF N=1 P=N:GOTO 110
55 IF M-N<2 THEN N=M
60 FOR I=2 TO N-1
65 R(I)=M-I+1
70 IF Q=1 GOTO 80 ELSE P=M*R(I)
75 Q=1:GOTO 90
80 P=P*R(I)
90 NEXT I
100 P=P*(M-N+1)
110 PRINTM;"P";N"="P
```

# **Sample Permutation Problems**

Evaluate 7°5
INPUT M
? 7
INPUT N
? 5
7 P 5 = 2520
Evaluate 3°2
INPUT M
? 3
INPUT N
? 2
3 P 3 = 6

In this example you should notice that the program has changed the problem from  $3^P2$  to  $3^P3$ . This is a special case and the program changes N from 2 to 3. To check the answer

$$\frac{-3!}{1!} = \frac{3 \cdot 2 \cdot 1}{1} = 6.$$

#### **COMBINATIONS**

The difference between combinations and permutations is that a combination is *without* regard to order. For example, in the group of letters X, Y, and Z, there are 6 permutations (XY, YX, XZ, ZX, YZ, ZY). With XY and YX there is only 1 combination, XY. So, for the letters X, Y, and Z, there are 3 combinations, XY, XZ, and YZ.

The equation for combinations is:

$$M^{C}N = \frac{M!}{(M-N)! \cdot N!}$$

# **Combination Program**

```
5 'COMBINATIONS
10 CLS
20 PRINT"INPUT M":INPUT M
30 PRINT"INPUT N": INPUT N
35
  IF M-N<N THEN N=M-N
40 IF N=0 C=1:GOTO130
50 IF N=1 C=M:GOTO130
60 R(1)=M-N+1
70 FOR I=2 TO N-1
80 R(I) = (M-N+I)/I
90 IF Q=1 GOTO 100ELSE C=R(1)*R(I)
95 Q=1:GOTO 110
100 C=C*R(I)
110 NEXT I
12Ø C=C*(M/N)
130 PRINTM;;"C";N"="C
```

# **Sample Combination Problems**

In how many ways can a group of 3 people be chosen from a larger group of 10 people? ( $10^{\circ}3$ )

INPUT M

? 10

INPUT N

?3

 $10 \,\mathrm{C} \,3 = 120$ 

There are 120 different ways to choose the 3 people for the smaller group.

A box contains 4 cards numbered 1 through 4. If 3 cards are drawn from the box, how many different combinations of numbers are possible?

INPUT M

?4

INPUT N

?3

4C3 = 4

#### ARITHMETIC MEAN

The arithmetic mean or common average of a set of numbers is the sum of those numbers divided by the quantity of numbers. For example, in the arithmetic mean, you would be asked to determine the mean of 2, 4, 3.1, 5, 6.7, 9, a total of 6 different numbers. The mean is the sum of these numbers divided by 6. Or, more specifically,

$$M = \frac{1}{n} \sum_{i=1}^{n} a_{i}$$

where the numbers are represented as  $a_1, a_2, a_3, \ldots a_n$ .

# **Arithmetic Mean Program**

- 5 'ARITHMETIC MEAN
- 10 CLS
- 20 PRINT"ENTER NUMBERS FOR THE ARI THMETIC MEAN"
- 30 INPUT N\$
- 40 IF N\$="/" GOTO 90
- 50 N=VAL(N\$)
- 60 A=A+N
- 7Ø X=X+1
- 80 GOTO 30
- 90 PRINT"THE ARITHMETIC MEAN IS"A/

# Sample Arithmetic Mean Problems

Determine the mean of 2, 4,3. 3.1, 5, 6.7, 9 (note that in the use of this program a / is used to denote the end of the information).

## ENTER NUMBERS FOR THE ARITHMETIC MEAN

```
? 2
? 4
? 3.1
? 5
? 6.7
? 9
```

?/

#### THE ARITHMETIC MEAN IS 4.9667

Population figures list the following as the number of children from the different families in a small rural town, 2, 4, 1, 5, 3, 10, 0, 6. What is the arithmetic mean for these families?

# ENTER NUMBERS FOR THE ARITHMETIC MEAN

```
?2
?4
?1
?5
?3
?10
?0
?6
```

## THE ARITHMETIC MEAN IS 3.875

You'll note that even through the seventh family did not have any children, they were counted in the total number of families (8).

## **GEOMETRIC MEAN**

The geometric mean is another type of average based on determining a specific root of a set of numbers. Using the same set of numbers 2, 4, 3.1, 5, 6.7, 9, the geometric mean is determined from the sixth root of the product of the numbers. More specifically,

$$A = {}^{n}\sqrt{n_{1} \cdot n_{2} \cdot n_{3} \dots n_{n}}$$

## **Geometric Mean Program**

- 5 'GEOMETRIC MEAN
- 10 CLS
- 20 PRINT" eNTER NUMBERS FOR THE GEO METRIC MEAN"
- 25 A=1
- 30 INPUT N\$
- 40 IF N\$=OPEN/" GOTO 90
- 50 N=VAL(N\$)
- 60 A=A\*N
- 70 X = X + 1
- 8Ø GOTO 3Ø
- 90 PRINT"THE GEOMETRIC MEAN IS"A\*(
  1/X)

## **Geometric Mean Sample Problems**

Determine the geometric mean of the examples given in the Arithmetic Mean section -2, 4, 3.1, 5, 6.7, 9 and 2, 4, 1, 5, 3, 10, 0.6.

#### ENTER NUMBERS FOR THE GEOMETRIC MEAN

? 2 ? 4

? 3.1

?5

?6.7

29

?/

#### THE GEOMETRIC MEAN IS 4.42205

Note the difference between the arithmetic and geometric means — 4.9667 vs. 4.42205.

# ENTER NUMBERS FOR THE GEOMETRIC MEAN

? 2

?4

25

?3

? 10

?0

26

?/

#### THE GEOMETRIC MEAN IS Ø.

This example was selected to illustrate that when trying to determine a geometric mean you must have some amount for each data sample. In other words, zero is not valid data. Referring back to the equation that solves for the geometric means, we see that a zero forces a zero product. Deleting the zero produces:

# ENTER NUMBERS FOR THE GEOMETRIC MEAN

?2 ?4

?1

?5

23

? 10

?6

?/

THE GEOMETRIC MEAN IS 3,5567

The arithmetic mean would be 4.41857.

#### HARMONIC MEAN

The last type of mean to be illustrated is the harmonic mean. Instead of being based on either a sum or product as in the arithmetic and geometric mean, the harmonic mean uses the reciprocals of the numbers in the data set. The formula for the harmonic mean is:

$$M = \frac{n}{\sum_{i=1}^{n} \sum_{i=1}^{i} a_{i}}$$

(where numbers are  $a_1, a_2, a_3 \dots a_n$ )

# **Harmonic Mean Program**

5 'HARMONIC MEAN

10 CLS

20 PRINT"ENTER NUMBERS FOR THE HAR MONIC MEAN"

30 INPUT N\$

40 IF N\$="/" GOTO 90

50 N=VAL(n\$)

60 A = A + (1/N)

7Ø X=X+1

80 GOTO 30

90 PRINT"THE HARMONIC MEAN IS"1/(A /X)

# Sample Harmonic Mean Programs

Using the numbers from the examples in the geometric mean section, determine the harmonic mean.

```
ENTER NUMBERS FOR THE HARMONIC MEAN
```

?2

?4

?3.1

? 5

? 6.7

?9

?/

## THE HARMONIC MEAN IS 3.91403

ENTER NUMBERS FOR THE HARMONIC MEAN

?2

?4

?1

?5

?3

? 10

?6

?/

# THE HARMONIC MEAN IS 2.7451

You'll again note that since reciprocals are being used, zero is invalid data since it would force a division by zero.

For the original set of data, 2, 4, 3.1, 5, 6.7, and 9, the means are:

arithmetic - 4.96670

 ${\tt geometric-4.42205}$ 

harmonic — 3.91403

#### **GROUPED DATA MEAN**

There is one other type of mean that will find use in other programs, the mean of grouped data. Instead of finding the mean of fifty individual numbers, the numbers are grouped into specific categories. For example:

category	number
10-19	14
20-29	14
30-39	22
	50

Mechanically, the mean of this grouped data is found by determining the midpoint of each group, multiplying this midpoint by the number in that group to produce a category product, summing the category products, and finally dividing this sum by the total number:

category	number	midpoint	category product
10-19	14	14.5	203
20-29	14	24.5	343
30-39	22	34.5	759
	50		1305

The mean of this grouped data is 1305/50 = 26.1. The actual formula is:

$$Mean = \frac{\sum mc}{n}$$

where n is the number of pieces of data and mc is the category product.

# **Mean Grouped Data Program**

- 5 'MEAN GROUPED
- 10 CLS
- 20 PRINT"ENTER THE RANGE OF THE PA RTICULAR CLASS (HIGHEST, LOWEST)
- 25 INPUT N\$(2),N\$(1)-
- 30 IF N\$(2)="/" GOTO100
- 40 PRINT"ENTER THE NUMBER WITHIH T HIS CLASS"
- 45 INPUT N\$(3)

50 N1=VAL(N\$(1)):N2=VAL(N\$(2)):N3=
VAL(N\$(3))
60 M=((N2-N1)/2)+N1
70 A=(N3\*M)+A
80 NT=NT+N3
90 GOTO 20
100 PRINT"THE MEAN IS"A/NT

# **Grouped Data Examples**

The time between repairs of various city buses is:

time	number of buses
0-7	34
8-14	12
15-21	56
22-28	7

Find the mean time between repairs (to indicate the end of data, enter /, / for the range).

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 7.0

ENTER THE NUMBER WITHIN THIS CLASS

? 34

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 14.8

ENTER THE NUMBER WITHIN THIS CLASS

? 12

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 21.15

ENTER THE NUMBER WITHIN THIS CLASS

? 56

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 28.22

ENTER THE NUMBER WITHIN THIS CLASS

? 7

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?/./

THE MEAN IS 13.156

Therefore, for the 109 buses in the city, each bus averaged 13.156 days between needed repairs.

Another example is one that is often seen in evaluations. Students in an Introduction to Drama course were asked to grade their instructor on a scale of 1 to 5 as to the value they received from that course, with 1 indicating little or no value and 5 indicating tremendous value. The evaluations produced the following information:

12.

Score — 1 2 3 4 5 Number — 15 8 9 3 21

What is the mean rating on this course?

Since the scores represent the actual midpoints of five infinitely small categories, the range information can be arbitrarily entered as plus or minus 1 from the midpoint. In other words, for the score 1, enter 2.0.

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?2,0

ENTER THE NUMBER WITHIN THIS CLASS

? 15

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?3,1

ENTER THE NUMBER WITHIN THIS CLASS

28

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?4,2

ENTER THE NUMBER WITHIN THIS CLASS

?9

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 5,3

ENTER THE NUMBER WITHIN THIS CLASS

?3

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?6,4

ENTER THE NUMBER WITHIN THIS CLASS

?21

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?/,/

THE MEAN IS 3.125

# STANDARD DEVIATION (UNGROUPED DATA)

The various types of means have been used to determine the center of specific groups of data. The next most commonly requested piece of information is the amount of variability or the spread of the data. This standard deviation is based on the amount of variance from the mean of the data. Standard deviation is measured in the same units as the scores, whereas variance, the basis for standard deviation, is measured in the scores squared, i.e., s² is the symbol for variance and s is the symbol for standard deviation. The recognized formula for standard deviation is:

$$S = \sqrt{\frac{\sum (\overline{x} - \overline{x})^2}{n-1}}$$

## **Standard Deviation Program**

```
5 'STANDARD DEV
```

10 CLS

20 PRINT"ENTER NUMBERS FOR THE STA NDARD DEVIATION (UNGROUPED DATA )"

30 INPUT N\$

4Ø IF N\$="/" GOTO 1ØØ

50 N=VAL(N\$)

60 A=A+N

70 X=NE 2+X

8Ø Y=Y+1

90 GOTO 30

100 PRINT"THE STANDARD DEVIATION I S"SQR((X-A+2/Y)/(Y-1))

# **Sample Standard Deviation Problems**

THE STANDARD DEVIATION IS 3.18198

```
Find the standard deviation for the data 2, 4, 3, 1, 5, 6, 7, 9.
ENTER NUMBERS FOR THE STANDARD DEVIATION (UN-
GROUPED DATA)
?2
?4
?3.1
?5
?6.7
?9
?/
THE STANDARD DEVIATION IS 2.54925
   Find the standard deviation for the data 2, 4, 1, 5, 3, 10, 0, 6.
ENTER NUMBERS FOR THE STANDARD DEVIATION (UN-
GROUPED DATA)
?2
?4
?1
?5
?3
?10
9.0
?6
?/
```

## STANDARD DEVIATION (GROUPED DATA)

Standard deviation for grouped data is determined in much the same way as the mean of grouped data and standard deviation. To explain, as in the mean of grouped data, a midpoint of each class is determined and then used in the standard deviation formula. This formula is:

$$S = \sqrt{\frac{\sum f(\overline{x} - \overline{x})^2}{n-1}}$$

## Standard Deviation (Grouped Data) Program

- 5 'STANDARD DEV. GROUPED
- 10 CLS
- 20 PRINT"ENTER THE RANGE OF THE PA RTICULAR CLASS (HIGHEST, LOWEST)
- 25 INPUT N\$(2),N\$(1)
- 30 IF N\$(2)="/# IF110
- 40 PRINT"ENTGR THE NUMBER WITHIN T HIS CLASS"
- 45 INPUT N\$(3)
- 50 N1=VAL(N\$(1)):N2=VAL(N\$(2)) N3=VAL(N\$(3))
- 60 M=((N2-N1)/2)+N1
- 70 A=(N3\*M)+A
- 80 B = (N3\*M\*M) + B
- 90 NT=NT+N3
- 100 GOTO 20
- 110 PRINT"THE STANDARD DEVIATION I S"LOG((B-A\*2/NT)/(NT-1))

### Sample Problems for Standard Deviation (Grouped Data)

Again, the time between repairs of various city buses is:

time	number of buses
0-7	34
8-14	12
15-21	56
22-28	7

Determine the standard deviation.

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 7.0

ENTER THE NUMBER WITHIN THIS CLASS

? 34

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 14.8

ENTER THE NUMBER WITHIN THIS CLASS

? 12

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 21,15

ENTER THE NUMBER WITHIN THIS CLASS

? 56

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

? 28,22

ENTER THE NUMBER WITHIN THIS CLASS

? 7

ENTER THE RANGE OF THE PARTICULAR CLASS (HIGHEST, LOWEST)

?/./

THE STANDARD DEVIATION IS 7.1504

#### LINEAR REGRESSION

The next three programs deal with the investigation of the relationship between two variables. Considering the two variables X and Y, what mathematical formula best describes the relationship between the given points? This first program will deal with linear regression, or a set of data points or a curve that approximates a straight line. The general equation for a straight line is Y = MX + B. From the data points it will be necessary to solve for the constants M and B which give the closest agreement. In addition to providing the constants, the program also solves for the coefficient of determination, a measure that indicates how closely the equation fits the initial data. The coefficient of determination is between 0 and 1, and the closer it is to 1 the better the equation fits.

Solving for the constants uses a method of least squares. The equations are:

$$S = \frac{\sum_{xy} - \frac{\sum_{x} \sum_{y}}{n}}{\sum_{x^{2}} - \frac{(\sum_{x})^{2}}{n}}$$

$$T = \overline{y} - S \overline{X}$$

$$where \overline{y} = \frac{\sum_{y}}{n}$$

$$\overline{x} = \frac{\sum_{x}}{n}$$

$$R = \frac{\left(\sum_{xy} - \frac{\sum_{x} \sum_{y}}{n}\right)}{\left(\sum_{y}^{2} - \frac{(\sum_{y})^{2}}{n}\right)} \left(\sum_{y}^{2} - \frac{(\sum_{y})^{2}}{n}\right)$$

# **Linear Regression Program**

5 'LINEAR REGRESSION

10 CLS

20 PRINT"ENTER THE GROUPS OF DATA POINTS (X,Y)

- 30 INPUT N\$(1);N\$(2)
  40 IF N\$(1)="/" GOTO 110
  50 N1=VAL(N\$(1)):N2=VAL(N\$(2))
  60 A=N1\*N2+A
  70 XT=N1+XT
  80 YT=N2+YT
  90 XS=N1\*N1+XS
  95 YS=N2\*N2+YS
  100 X=X+1
  105 GOTO 30
  110 S=(A-(XT\*YT/X))/(XS-((XT\*2)/X))
  )
  120 T=YT/X-(S\*(XT/X))
  130 R=(X\*A-(XT\*YT))/(SQR(X\*XS-(XT\*2))\*(SQR(X\*YS-(YT\*2))))
- 140 PRINT"FOR THE GENERAL EQUATION Y=MX+B, M="S"AND B="T"."CHR\$(13)"THE COEFFICIENT OF DETERMINATION IS"RI2

# **Sample Linear Regression Problems**

You want to use a thermometer to measure the outside temperature at the top of a mountain. Unfortunately, the only thermometer that you can buy locally is measured in Centigrade. However, you do have an inside thermometer which is marked in Fahrenheit, but it only goes down to freezing, 32 degrees. How do you measure the outside temperature?

One method might be to immerse both thermometers in a bowl of very hot water and record the temperatures of both thermometers as the water cools. From this information, you could determine the exact relationship between the two thermometers and calculate the outside temperature in Fahrenheit.

The readings as the water cools are:

Fahrenheit	Centigrade
180	82
142	61
133	56
105	40
90	32
73	23
64	18
50	10

### ENTER THE GROUPS OF DATA POINTS (X, Y)

?82,180

?61,142

? 56, 133

?40,105

? 32,90

. 02,00

? 23,73

? 18,64 ? 10,50

?/,/

FOR THE GENERAL EQUATION Y=MX+B, M=1 1.80864 AND B=31.8274.

# THE COEFFICIENT OF DETERMINATION IS . 999922

This example was selected since the conversion equation between Centigrade and Fahrenheit is well known (F = 1.8C + 32) and readily fits the general equation for a straight line. Linear regression can be used in many ways to help correlate/extrapolate data. Consider Fig. 3-1 and find the equation that best describes the data.

#### ENTER THE GROUPS OF DATA POINTS (X, Y)

? 1.25, 1.1

?3,3.4

?4.5,5.2

?6,7.2

?/./

FOR THE GENERAL EQUATION Y=MX+B, M=1.27648 AND B=-.482017

# THE COEFFICIENT OF DETERMINATION IS . 999636

So, from the four selected data points, the general equation of a line that best describes the data has been determined. From this line and equation, the data can be extrapolated out through values of 12 for X.

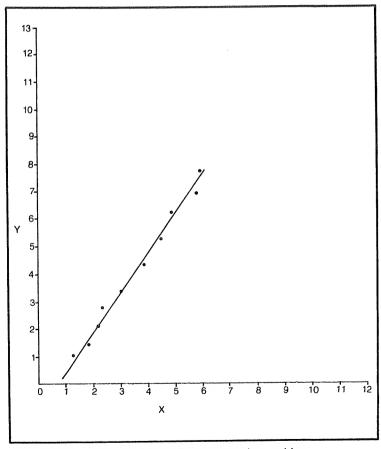


Fig. 3-1. To be used in solving a linear regression problem.

$\boldsymbol{X}$	Y
1	.79
2	2.07
3	3.35
8	9.73
9	11.01
10	12.28
11	13.56
12	14.84

#### LOGRITHMIC CURVE FIT

This next program is very similar to linear regression, except that, instead of being a straight-line type of relationship, it is a function of the natural  $\log$  (e) of X. Fitting to a logrithmic curve uses the general equation  $Y = M \ln X + B$ . The logrithmic curve is a typical form in that one axis of the curve is compressed in relation to the other. The following examples will clearly show this relationship. The equations used to solve for the logrithmic curve fit are:

$$S = \frac{\sum y \ln x - \frac{1}{n} (\sum \ln x \sum y)}{\sum (\ln x)^2 - \frac{1}{n} (\sum \ln x)^2}$$

$$T = \frac{1}{n} (\sum y - \sum \ln x)$$

$$R = \frac{(\sum y \ln x - \frac{1}{n} (\sum \ln x \sum \ln y))^2}{(\sum (\ln x)^2 - \frac{1}{n} (\sum \ln x)^2) (\sum y^2 - \frac{1}{n} (\sum y)^2)}$$

# **Logrithmic Curve Fit Program**

```
5 'LOG CURVE FIT
10 CLS
20 PRINT"ENTER THE GROUPS OF DATA
    POINTS (X,Y)
30 INPUT N$(1),N$(2)
40 IF N$(1)="/" GOTO 130
50 N1=VAL(N$(1)):N2=VAL(N$(2))
60 A=A+N2*LOG(N1)
70 B=B+LOG(N1)
75 I=I+N2
80 C=C+(LOG(N1))*2
85 F=F+N2*2
70 G=G+LOG(N1)
100 D=B*2
```

- 110 X = X + 1
- 120 GOTO 30
- 130 E=(A-B\*I/X)/(C-D/X)
- 140 H = (I E \* G) / X
- 150 PRINT"iN THE GENERAL FORM OF Y =M(LN(X))+B, M="E"AND X="H"."
- 160 J=((A-B\*I/X)\*2)/((C-D/X)\*(F-((I\*2)/X)))
- 165 PRINT"THE COEFFICIENT OF DETER MINATION IS"J

# Sample Logrithmic Curve Fit Problems

Determine the equation of the line shown in Fig. 3-1. As can be seen, the curve can not be stretched to produce a straight line and the data points seem to compress as the values for X get bigger. Therefore, this is a good candidate for logrithmic curve fit program. Four data points were selected.

If the coefficient of determination is not high enough, additional points can be selected and the program run again.

ENTER THE GROUPS OF DATA POINTS (X, Y)

? 2,.5

?4,1.5

? 6.3,2.25

? 9.5.2.75

?/,/

IN THE GENERAL FORM OF Y+M(LN(X))+B, M=1.46487 AND B=-.510028.

THE COEFFICIENT OF DETERMINATION IS . 997925.

Again, with four point, you have been able to determine the equation of the line that produces the best fit through the data points. More points could have been added, though it is a matter of diminishing returns as to whether the additional time is worthwhile for the small increase in accuracy. For example, adding the additional points 1.45,0 and 7.5,2.5 changes M to 1.48962, X to -.541302, and raises the coefficient of determination to .998624, a very small change in accuracy rating. The actual equation of the line for this example was Y = 1.51nX - 0.5.

#### **EXPONENTIAL CURVE FIT**

The last curve fit program is for data that exhibits an exponential type of progression. You'll notice that the curve in Fig. 3-3 is somewhat similar to that of Fig. 3-2 in that it seems to approach some limit. This is a case where it might be easiest to run the data set in both the exponential and logrithmic curve programs to determine the best fit. However, in some cases, inferences can be made because of the data range to help select the appropriate program to use.

The equations to solve the exponential curve fit problem are:

$$S = \frac{\sum x \ln y - \frac{1}{n} (\sum x) (\sum / ny)}{\sum x^2 - \frac{1}{n} (\sum x)^2}$$

$$T = EXP \left(\frac{\sum \ln y}{n} - S \frac{\sum x}{n}\right)$$

$$R = \frac{(\sum x \ln y - \frac{1}{n} (\sum x \sum \ln y))^2}{\left((\sum x^2 - \frac{(\sum x)^2}{n}\right) \left((\sum (\ln y)^2 - \frac{(\sum \ln y)^2}{n}\right)\right)}$$

# **Exponential Curve Fit Program**

90 F=D[2

```
5 'EXP. CURVE FIT
10 CLS
20 PRINT"ENTER THE GROUPS OF DATA
    POINTS (X,Y)
30 INPUT N$(1),N$(2)
40 IF N$(1)="/" GOTO 130
50 N1=VAL(N$(1)):N2=VAL(N$(2))
60 A=A+N1*LOG(N2)
70 B=B+LOG(N2)
75 I=I+N1
80 C=C+N1*2
85 D=D+N1
```

- 100 G=G+(LOG(N2) 42)
- 110 X = X + 1
- 120 GOTO 30
- 130 E = (A E \* I / X) / (C F / X)
- 140 H=EXP(B/X-E\*I/X)
- 150 PRINT"IN THE GENERAL FORM OF Y =M\*ECBX, M="E"AND X="H"."
- 160 J=((A-B\*I/X)\*2)/((C-F/X)\*(G-((BC2)/X)))
- 165 PRINT"THE COEFFICIENT OF DETER MINATION IS"J

### Sample Exponential Curve Fit Problem

Using Fig. 3-3, solve for the equation that best describes the line in the data points.

X	Y
1	.9
3	.35
5	.13
7	.04

ENTER THE GROUPS OF DATA POINTS (X, Y)

?1..9

?3..35

? 5,.13

? 7..04

?/,/

IN THE GENERAL FORM OF Y=M\*E!BX, B=-.516547 AND M=1.58822.

THE COEFFICIENT OF DETERMINATION IS . 997247.

Running the same data set in the logrithmic curve fit program produces: B= .881006 and M=-.452093 and a coefficient of determination of .991973. Since the two coefficients of determination are so close, it might be wise to use additional points to find the best fit. However, using more data points is not without its problems. Since there are more points, the amount of error tends to reduce the coefficients of determination.

For example, consider the following data set:

$\boldsymbol{X}$	$\boldsymbol{Y}$
1	.9
3	.35
5	.13
7	.04
2	.51
6	.75
10	.015

When applied to the exponential curve fit program, B now equals -.421978, M=1.48592, and the coefficient of determination is .71439. You'll notice that even though the changes in B and M are relatively small, the coefficient of determination has decreased significantly. With the increased number of data points, any error is now more significant. For comparison, when using the logrithmic curve fit program, B=.32053, M=.817324, and the coefficient of

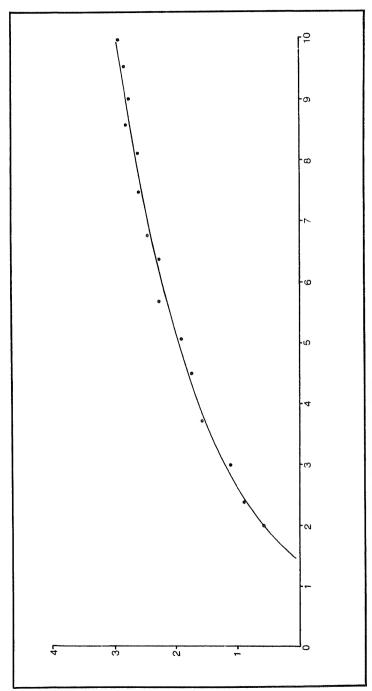
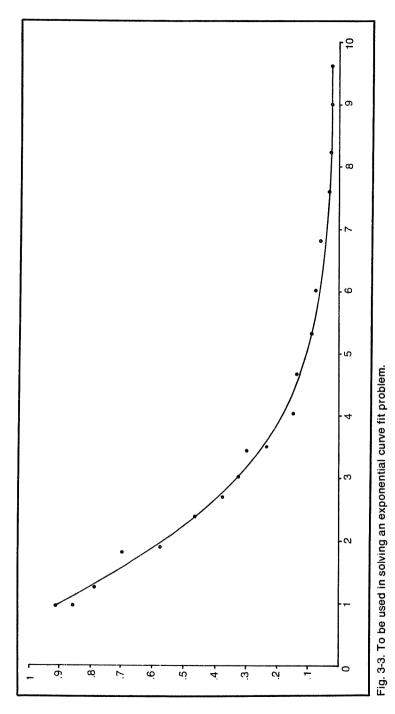


Fig. 3-2. To be used in solving a logrithmic curve fit problem.



determination is .536147. So, increasing the number of data points has lowered the confidence levels overall for B and M, yet they have provided greater assurance that the correct curve fit program is being used.

# **FACTORIAL**

As mentioned earlier in this chapter, a factorial, N, is the simple progression N  $\bullet$  (N-1)  $\bullet$  (N-2) . . . (2)  $\bullet$  (1). Integers must be used.

# **Factorial Program**

- 5 'FACTORIAL
- 10 CLS
- 20 INPUT"ENTER AN INTEGER"; N
- 30 M=1
- 40 FOR I=1 TO N
- 50 M=M\*I
- 60 NEXT I
- 70 PRINT"THE FACTORIAL OF"N"IS"M

# Sample Factorial Problems

ENTER AN INTEGER
? 9
THE FACTORIAL OF 9 IS 362880
ENTER AN INTEGER
? 24
THE FACTORIAL OF 24 IS 6.20448E+23

#### **CHI-SQUARE EVALUATION**

The last program in this chapter deals with chi-square tests or evaluations. This evaluation can be used to determine two pieces of information: "goodness of fit," and where two variables are related or independent. Since this is not a book devoted to statistics, but one that shows how many different types of programs can be computerized for everyday use, I am not going to explain the complete procedure for using the chi-square evaluation. However, this program will solve for chi-square, which can then be used to determine goodness of fit and any relationship between variables.

The chi-square evaluation calculates the relationship between the observed frequency and the expected frequency in the distribution of samples. The formula is:

$$X^2 \Sigma \frac{(O_i - E_i)^2}{E_i}$$

# **Chi-Square Evaluation Program**

5 'CHI-SQUARE EVAL.

10 CLS

20 PRINT"ENTER THE OBSERVED FREQUE NCY, EXPECTED FREQUENCY INFORMATION"

25 INPUT O\$,E\$

3Ø IF O\$="/" GOTO7Ø

40 0=VAL(0\$):E=VAL(E\$)

5Ø KI=KI+((O-E) 42)/E

60 GOTO 25

70 PRINT"THE CHI-SQUARE EVALUATION IS"KI

# **Chi-Square Sample Problems**

Determine Chi-Square for the following information.

Observed	Expected
20	30
60	90
110	120
50	30
60	30

ENTER THE OBSERVED FREQUENCY, EXPECTED FREQUENCY INFORMATION

? 20,30

? 60,90

? 110,120

? 50,30

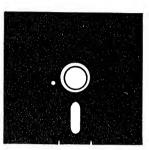
? 60,30

?/,/

THE CHI-SQUARE EVALUATION IS 57.5

As I said, this information will now be used to determine whether the assumed hypothesis is true or false.

# Chapter 4 Electronics Programs



This next chapter is devoted to programs encountered in many facets of electrical engineering. Admittedly, there are an infinite number of equations used in the field of electrical engineering, but these programs represent a fair cross section. There are also programs which might not ordinarily be at one's fingertips for instant use. In this chapter I will start going into detailed explanations of the programs themselves. So far in this book, the programs have generally not been sufficiently complicated to warrant a closer examination. However, in this chapter, a number of programs contain smaller programs which can be used either singly or in combinations to solve other problems.

#### **ANTENNA PATTERN**

This first program of the chapter will be used to determine the radiation pattern of vertical antennas. In many cases, the radiation pattern can be found by checking any of the many reference texts available which show patterns for "common" antenna configurations. The problem arises when certain factors dictate antenna positioning that does not fall into a common configuration. At such a time this program proves invaluable.

To compute the radiation pattern from a group of vertical radiators requires that you know the antenna spacing, phase difference, individual antenna currents, and positional location between the antennas. Figure 4-1 shows a diagram that will be used to explain the designations used in the program. In this diagram there are three antennas, with one designated as the reference antenna. The other two are located both in spacing and distance from this reference antenna. In addition to the physical positions, the second two antennas are related to the reference by their individual antenna currents and phase. The four designators for the antennas are:

Antenna Current	С
Phase relationship to the reference	P
Spacing from the reference	S
Angular Displacement from the reference	AD

The last quantity, angular displacement, is used to orient the pattern in either a relative or true plane. To explain, if you are only concerned with the pattern relative to the antennas, use zero as the angular displacement for Antenna 1 and 60 degrees as the angular displacement for Antenna 2 (see Fig. 4-1). If you want to determine the pattern base on True North, use the actual true bearing from the reference to the selected antenna. Lines 50 through 150 of the Antenna Pattern program are used to input this data. The first input statement, line 20, sets the number of points at which the data will be plotted. In effect, it determines the number of times the pattern information will be summed. Line 50 inputs the total number of verticals in the antenna system. Note that this value, E, is decreased by 1 to take into account the reference element. The complete equation to determine the antenna pattern is:

$$\mathbf{A}(\theta) = \big| + \sum_{\mathbf{n}=1}^{\mathbf{N}-1} \mathbf{A}_{\mathbf{n}}^{\mathbf{1}} \, \mathbf{e} \, \mathbf{j}^{\mathbf{d}\mathbf{n}} \, \big|$$

Lines 160 through 270 of the program do the actual summing to determine the relative amplitude of the pattern for each plotting point. Note that in lines 200 and 210 the formula for resolving a polar form of notation to rectangular coordinates is used. The respective X and Y quantities are then summed in lines 220 and 230 each time through the loop. Once the required number of loops have been completed, as determined by the number of elements, line 260 converts the X and Y information back to a polar notation. From here, line 270 returns back to line 170 to repeat this entire process for the next plotting point.

Lines 275-430 show the display portion of the program. In this section, the information is formatted into three columns for presentation. Lines 271 through 300 display the information in a relative amplitude format. More useful than the relative amplitude format is one that presents the information after being normalized to the largest value. This program will present either normalized data or normalized data expressed in dB. Lines 310 and 320 search the information file to determine the largest value for use in the normalized data.

#### **Antenna Pattern Program**

- 5 ANTENNA PATTERN
- 10 CLS
- 20 INPUT "ENTER NUMBER OF DEGREES BETWEEN PLOTTING POINTS";D

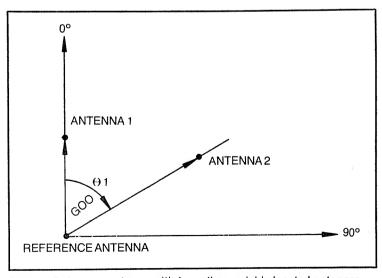


Fig. 4-1. Reference antenna with two other variably located antennas.

- 30 DIMN(360/D)
- 35 PRINT
- 45 PRINT"THE REFERENCE ELEMENT IS DESIGNATED AS ELEMENT 0"
- 49 PRINT
- 50 INPUT"ENTER THE TOTAL NUMBER OF ELEMENTS":E
- 55 PRINT
- 60 E=E-1
- 70 FOR I=1 TO E
- 80 PRINT"FOR ELEMENT"I"ENTER THE A NTENNA CURRENT."
- 90 INPUT C(I)
- 100 PRINT"ENTER THE PHASE DIFFEREN CE BETWEEN ELEMENT"I"AND THE R EFERENCE"CHR\$(13)"ELEMENT."
- 101 PRINT"USE + FOR LAGGING AND FOR LEADING."
- 110 INPUTP(I)
- 120 PRINT"ENTER THE SPACING IN DEG REES (ONE WAVELENGTH = 360 DEG REES)"CHR\$(13)"BETWEEN ELEMENT "I"AND THE REFERENCE"
- 130 INPUTS(I)
- 140 PRINT"ENTER THE ANGULAR DISPLA CEMENT IN DEGREES BETWEEN THE REFERENCE"CHR\$(13)"ELEMENT AND ELEMENT"I
- 150 INPUT AD(I)
- 160 NEXT I
- 170 FOR J=0 TO 360STEP D
- 180 FOR I=1 TO E
- 185 M=COS((J-AD(I))/57.29578)
- 190 G=S(I)\*M-P(I)
- 200 X=C(I)\*COS(G/57.29578)
- 210 Y=C(I)\*SIN(G/57.29578)
- 220 XS=XS+X
- 230 YS=YS+Y
- 240 NEXT I
- 250 XS=XS+1
- 255 F=J/D
- 260 N(F) = S0R(XS[2+YS[2)]

- 261 XS=Ø
- 262 YS=0
- 270 NEXT J
- 271 CLS
- 275 PRINTTAB(9)"MAG."TAB(29)"MAG."
  TAB(50)"MAG."
- 280 FOR Q=0 TO 110 STEP D
- 295 PRINT@+DTAB(5)"DEG"TAB(8)N((@+D)/D)TAB(20)@+D+120TAB(25)"DEG"TAB(25)"DEG"TAB(28)N((@+D+120)/D)TAB(41)G+D+240TAB(46)"DEG"TAB(49)N((@+D+240)/D)
- 300 NEXT 0
- 310 FOR R=0 TO 360/D
- 320 IF N(R)>NG THEN NG=N(R):NEXT R ELSE NEXT R
- 34Ø INPUT"DO YOU WANT NORMALIZED D
  ATA?";ND\$
- 345 IF ND\$="Y"GOTO 347
- 346 END
- 347 CLS
- 348 PRINTTAB(9)"MAG."TAB(29)"MAG."
  TAB(50)"MAG."
- 350 FOR Q=0 TO 110 STEP D
- 360 PRINT@+DTAB(5)"DEG"TAB(8)N((@+D)/D)/NGTAB(20)@+D+120TAB(25)"DEG"TAB(28)N((@+D+120)/D)/NGTAB(41)@+D+240TAB(46)"DEG"TAB(49)N((@+D+240)/D)/NG
- 370 NEXT Q
- 380 INPUT"DO YOU WANT NORMALIZED D
  ATA EXPRESSED IN DB?";DB\$
- 390 IF DB\$="Y"THENGOTO 400
- 395 END
- 400 CLS
- 410 PRINTTAB(9)"DB"TAB(29)"DB"TAB(50)"DB"
- 415 FOR Q=Ø TO 11Ø STEP D
- 420 PRINT@+DTAB(5)"DEG"TAB(8)20\*(L OG(N((@+D)/D)/NG)/LOG(10))TAB( 21)@+D+120TAB(27)"DEG"TAB(30)2 0\*(LOG(N((@+D+120)/D)/NG)/LOG(

101) TAB(43) Q+D+240TAB(47) "DEG" TAB(51)20\*(LOG(N((Q+D+240)/D)/ NG)/LOG(10)) 430 NEXT 0

Where

 $A(\theta)$  = pattern amplitude as a function of  $\theta$ 

 $A^1$  = relative amplitude of the nth element

 $\mathring{N}$  = total number of elements

 $\psi_{n} = \beta d_{n} \cos (\theta_{n} - \theta) - \alpha_{n}$   $\alpha_{n} = \text{phase of the nth element relative to the}$ reference element in degrees (+ for lagging,

- for leading phase)

 $\beta d_{a}$  = electrical distance (in degrees) from the driven element to the nth element

 $\theta$  = spatial angle between elements.

# Sample Antenna Pattern Problem

For this example, use Fig. 4-1. The spacing between the Reference Antenna and Antenna 1 is 0.5 wavelengths (180 degrees) and between the Reference and Antenna 2 is 1 wavelength. Antenna 2's angular displacement is 60 degrees. The current in Antenna 1 is 1 and in Antenna 2 is 2. The phase between the reference and Antenna 1 is 90 leading and between the reference and Antenna 2 is 180 degrees leading. Determine the normalized amplitude in dB every 30 degrees.

ENTER NUMBER OF DEGREES BETWEEN PLOTTING POINTS? 45

THE REFERENCE ELEMENT IS DESIGNATED AS ELE-MENT Ø

ENTER THE TOTAL NUMBER OF ELEMENTS? 3 FOR ELEMENT 1 ENTER THE ANTENNA CURRENT.

? 1

ENTER THE PHASE DIFFERENCE BETWEEN ELEMENT 1 AND THE REFERENCE ELEMENT. Use + FOR LAGGING AND - FOR LEADING.

? - 90

ENTER THE SPACING IN DEGREES (ONE WAVELENGTH = 360 DEGREES) BETWEEN ELEMENT 1 AND THE REFER-**ENCE** 

? 180

ENTER THE ANGULAR DISPLACEMENT IN DEGREES BETWEEN THE REFERENCE ELEMENT AND ELEMENT 1?  $\alpha$ 

FOR ELEMENT 2 ENTER THE ANTENNA CURRENT.

?2

ENTER THE PHASE DIFFERENCE BETWEEN ELEMENT 2 AND THE REFERENCE ELEMENT. USE + FOR LAGGING AND - FOR LEADING.

? - 180

ENTER THE SPACING IN DEGREES (ONE WAVELENGTH = 360 DEGREES)

BETWEEN ELEMENT 2 AND THE REFERENCE ? 360

ENTER THE ANGULAR DISPLACEMENT IN DEGREES BETWEEN THE REFERENCE ELEMENT AND ELEMENT 2 ? 60

MAG.	MAG.	MAG.
30 DEG .940224	150 DEG 1.08759	270 DEG . 593411
60 DEG 2	180 DEG 3.16228	300 DEG 2
90 DEG 2.51373	210 DEG 2.40561	330 DEG 1.67844
120 DEG 4	240 DEG 1.12352E-06	360 DEG 3.16228

# DO YOU WANT NORMALIZED DATA?? Y

MAG.	MAG.	MAG.
30 DEG .235056	150 DEG .271897	270 DEG.148353
60 DEG.5	180 DEG.790569	300 DEG.5
90 DEG .628432	210 DEG . 601402	330 DEG .419609
120 DEG 1	240 DEG 2.8088E-07	360 DEG . 79057

# DO YOU WANT NORMALIZED DATA EXPRESSED IN DB?? Y

MAG.	MAG.	MAG.
30 DEG-12.5766	150 DEG-11.3119	270 DEG-16.5741
60 DEG-6.0206	180 DEG-2.0412	300 DEG-6.0206
90 DEG-4.03484	210 DEG-4.4167	330 DEG-7.5431
120 DEG 0	240 DEG-131.03	360 DEG-2.04119

#### **GAMMA MATCH**

The next two programs are also antenna-related, being designed to provide matching information between an antenna and a transmission system. The first, the Gamma Match Program, will determine the necessary dimensions for a Gamma Match on the driven element of a Yagi antenna. However, the Yagi antenna is not the only applicable type of antenna. Vertical antennas can also be shunt fed using the same type of matching arrangement.

As with the last program on antenna patterns, this program uses many smaller operations to obtain the final answer, computing the impedance of two parallel conductors, polar to rectangular conversions, and Smith Chart operations. Again, the complete program will be explained in small sections so that you can understand the operations and use any portions for your own programs.

First, see Fig. 4-2. This diagram illustrates the gamma match and shows the designations used in the program. Each is relatively self-explanatory. Note that the spacing between the driven element and gamma rod is the spacing between the inner edges of the two pieces. Each of the spacings is entered in inches, the impedances in ohms, and the frequency in megahertz.

Lines 90 through 110 of the Gamma Match Program compute the impedance step-up ratio between the gamma rod and driven element by the following formula:

$$r = \left(1 + \frac{\log \frac{2S}{d_1}^z}{\log \frac{2S}{d_2}}\right)$$

where S = center-to-center spacing

d = diameter of driven element

 $d_{i}^{z} = diameter of rod$ 

This ratio must be computed to compensate for the unequal diameters of the element and gamma rod which act as a section of transmission line.

Since these two pieces do act as a section of transmission line that has been short circuited at one end, they will add some additional reactance that must be taken into account during the calculations. Line 120 computes the impedance of this section of transmission line. The formula for this equation is:

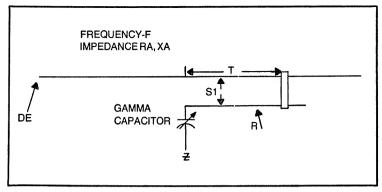


Fig. 4-2. The gamma match and designations used in the program.

$$Z_0 = 60 \cosh^{-1} \frac{45^2 - d_2^2 - d_1^2}{2 d_2 d_1}$$
 ohms

The next step is to determine the increased impedance of the driven element over its center-point impedance caused by its being fed off center (tap point of gamma rod). Line 130 does double duty by not only calculating this increased impedance, but also multiplies this product by the previously determined step-up ratio. At this point, RI and XI represent the real and imaginary components of the inital input impedance. Lines 140 and 150 calculate the impedance after the RI and XI values have been added to the reactance caused by the short-circuited section of the transmission line. These new values, RI(2) and XI(2), represent the real and imaginary components which will be rotated around the Smith Chart. The amount of rotation is determined by the length of the gamma rod vs. the frequency of operation. Lines 160, 170, and 180 perform the actual rotation calculations. The formula for this rotation is:

$$Z = \left(\frac{RI1 + jXI1}{RI2 + jXI2}\right) R_o$$

$$\begin{aligned} \text{where RI1} &= R_{\text{L}} \\ \text{XI1} &= R_{\text{o}}^{\text{o}} X_{\text{K}} + X_{\text{L}} \\ \text{RI2} &= R_{\text{o}}^{\text{o}} - X_{\text{L}} X_{\text{K}} \\ \text{XI2} &= R_{\text{I}}^{\text{o}} X_{\text{K}} \end{aligned}$$

The division performed in line 180 is a complex type of division. That is, it is performed in a polar notation by dividing the magnitudes and subtracting the phase angles.

The next group of lines starts by converting the M3 and A3 values back to the rectangular type of notation in line 190. Next, lines 210 and 220 convert the series equivalent of the impedance to a parallel equivalent. This is done so that the reactance caused by the short-circuited section of transmission line can be directly added to the parallel equivalent. Once this reactance is added, line 230, the parallel equivalent, is converted back to the series form in lines 240 and 260. And finally, the real part of the impedance is multiplied by the system impedance to produce the final real and imaginary parts.

In line 270, the final real part of the impedance is compared to the transmission system impedance. If the difference is less than 1 percent, the value of the gamma capacitor is calculated and displayed. Otherwise, the program will change the value of T, the distance to the tap point, and go through the entire series of calculations again. Initially, the change to T is one inch. However, once the difference is less than 5 ohms, but more than 1 percent, T is either incremented or decremented by 0.25 inch until a calculation shows a difference of less than 1 percent.

The final group of lines, lines 350 to the end, are used to change any of the initial parameters for recalculations.

# Gamma Match Program

'GAMMA MATCH

```
PRINT"PROGRAM WILL TAKE THE INITIAL DATA AND GO THROUGH MULTIPLE"
                                                                                                                              PRINT"THE FINAL TAP POINT WILL BE WITHIN ONE QUARTER OF AN INCH."
PRINT"THIS PROGRAM IS DESIGNED TO DETERMINE THE FINAL TAP POINT"
                                                                                                                                                               PRINT"THIS WILL PROVIDE A SUFFICIENTLY ACCURATE STARTING POINT"
                                                                                             PRINT"ITERATIONS UNTIL A SUITABLE MATCH HAS BEEN DETERMINED."
                              PRINT" AND VALUE OF THE SERIES CAPACITOR IN A GAMMA MATCH.
                                                                                                                                                                                                                                                                                                                                                                     RESISTIVE PORTION OF ANTENNA IMPEDANCE" RA
                                                                                                                                                                                                                                                                                                                                                                                                   "ENTER REACTIVE PORTION OF ANTENNA IMPEDANCE"; XA
                                                                                                                                                                                                                                                                                                 SPACING BETWEEN ELEMENT AND ROD"; S1
                                                                                                                                                                                                                                                                                                                                    TRANSMISSION SYSTEM IMPEDANCE";Z
                                                                                                                                                                                                                                "ENTER DIAMETER OF ELEMENT"; DE "ENTER DIAMETER OF GAMMA ROD"; DR
                                                                                                                                                                                                                                                                                                                                                                                                                                      "ENTER FREGUENCY IN MEGAHERTZ" ; F
                                                                                                                                                                                               PRINT"FOR AN ACTUAL ANTENNA, ": PRINT
                                                                                                                                                                                                                                                                                                 "ENTER
                                                                                                                                                                                                                                                                                                                                  "ENTER
                                                                                                                                                                                                                                                                                                                                                                     "ENTER
                                                                                                                                                                                                                                  LUDUI
                                                                                                                                                                                                                                                                                                                              INPUT
                                                                                                                                                                                                                                                                 INPUT
                                                                                                                                                                                                                                                                                                 INPUT
                                                                                                                                                                                                                                                                                                                                                                                                                                    INPUT
                                                                                                                                                                                                                                                                                                                                                                   INPUT
                                                                                                                                                                                                                                                                                                                                                                                                   INPUT
```

S=DE/2+DR/2+S1

100 Y=((4\*S\*S)+(DE+2)-(DR+2))/(4\*S\*DE):Y1=LOG(Y+S0R(Y\*Y-1))

X=((4\*5\*5)-(DE\*2)+(DR\*2))/(4\*5\*DR):X1=LOG(X+50R(X\*X-1))

INPUT "ENTER DISTANCE IN INCHES FROM CENTER OF DRIVEN ELEMENT TO CENTER OF GAMMA ROD SHORTING STRAP"; T: T(1)=T

```
ZL1=((4*S*S)-(DR42)-(DE42))/(Z*DE*DR):ZL=60*(LOG(ZL1+S0R(ZL1*ZL1-1
                                                                                RI=HZ*RA/(COS(T*F*5.32343E-04))42:XI=HZ*XA/(COS(T*F*5.32343E-04))4
                                                                                                                                                           RI(2)=ZL-(XI*TAN(T*F*5.32343E-Ø4)):XI(2)=RI*TAN(T*F*5.32343E-Ø4)
M1=((RI(1))*2+(XI(1))*2)*.5:A1=ATN(XI(1)/RI(1))*57.2958
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         IF ABS(RF-Z)<Z/100 PRINT"THE FINAL RESISTANCE IS";RF"(A DIF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     FERENCE OF LESS THAN 1 PERCENT). THE NEW TAP POINT IS AT";
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              T;"INCHES. THE GAMMA"CHR$(13)"CAPACITOR IS";1E6/(2*3.1416*
                                                                                                                                                                                                                                                    M2=((RI(2))42+(XI(2))42)4.5:A2=ATN(XI(2)/RI(2))*57.2958
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      RS(1)=M5*COS(A5*.01745329):XS(1)=M5*SIN(A5*.01745329)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  ABS(RF-Z)<5 T=T-.25:GOTO 130 ELSE T=T-1:GOTO 130 ABS(RF-Z)<5 T=T+.25:GOTO 130 ELSE T=T+1:GOTO 130
                                                                                                                                                                                                                                                                                                                                    RR=M3*COS(A3*.01745329):XR=(M3*SIN(A3*.01745329))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         RP=M4*COS(A4*.01745329):XP=M4*SIN(A4*.01745329)
                                                                                                                       RI(1)=RI:XI(1)=(ZL*TAN(T*F*5.32343E-04))+XI
                                                                                                                                                                                                                                                                                                                                                                                                                               M4=1/(XS42+RS[2)4.5:A4=-ATN(XS/RS)*57.2958
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            M5=1/(RP[2+XT42)[.5:A5=-ATN(XT/RP)*57.2958
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        F*XF);"PICOFARADS":GOTO 350 ELSE 272
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 ABS(RF-Z)<5 T=T+.25:GOTO 130
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     XT=XP+(-1/TAN(T*F*5.32343E-04))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    PRINTT" INCHES", RF" OHMS"
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    RF=ZL*RS(1):XF=ZL*XS(1)
                                                                                                                                                                                                                                                                                                M3=M1/M2:A3=A1-A2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                RF<Z GOTO 310
HZ=(1+X1/Y1)♦2
                                                                                                                                                                                                                                                                                                                                                                                      RS=RR:XS=XR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             290
```

```
PRINT"ENTER THE PARAMETER YOU WANT TO CHANGE"
                                                                                                                                                                                                                                               ANTENNA RESISTANCE?":INPUT
                                                                                                                                                                                                                                SYSTEM IMPEDANCE?":INPUT Z
                                                                                                                                                                                                                                                               ANTENNA REACTANCE?":INPUT
                                                                                                                                                                               ELEMENT DIAMETER?":INPUT
                                                                                                                                                                                               ROD DIAMETER?":INPUT DR
PRINT AGAIN? (1=YES, Ø=NO) ": INPUT @
                                                                                                                                                                                                                SPACING?":INPUT S1
                                                                                                                PRINTTAB(10)"ANTENNA RESISTANCE
                                                                                                                               PRINTTAB(10)"ANTENNA REACTANCE
                                                PRINTTAB(10)"ELEMENT DIAMETER
                                                                                                PRINTTAB(10)"SYSTEM IMPEDANCE
                                                                PRINTTAB(10)"ROD DIAMETER
                                                                                                                                                PRINTTAB(10)"FREGUENCY
                                                                                PRINTTAB(10)"SPACING
                                                                                                                                                                                PRINT"NEW
                                                                                                                                                                                               PRINT"NEW
                                                                                                                                                                                                                                                               PRINT"NEW
                                                                                                                                                                                                                                PRINT"NEW
                                                                                                                                                                                                                PRINT"NEW
                                                                                                                                                                                                                                              PRINT"NEW
                IF Q=0 THEN
                                                                                                                                                                INPUT N
                                                                                                                                                                                                Į
                                                                                                                                                                                                                                 7≡7
                                                                                                                                                                                                               N=3
                                                                                                                                                                                                                                                                 9<u>"</u>N
                                                                                                                                                                                                                                                N=5
                                                                                                356
                                                                                                                               358
                                                                                                                                                359
                                                                                                                                                                                 362
                                                                                                                                                                                                363
                                                                                                                                                                                                                364
                                                                                                                                                                                                                                365
                                                                                                                                                                                                                                                366
                                                                                                                                                                                                                                                                367
                                                                                                                  357
                                                                                                                                                               361
```

FREQUENCY?":INPUT F

PRINT"NEW

N=7

00

T=T(1):GOTO

# Sample Gamma Match Program

Determine the correct tap point and gamma capacitor value for an antenna and Gamma Match system with the following characteristics:

Driven Element Diameter	1 inch
Gamma Rod Diameter	.375 inch
Inside Spacing	4 inches
Transmission System Impedance	50 ohms
Real Part of Antenna Impedance	35 ohms
Imaginary Part of Antenna Impedance	-35  ohms
Frequency	16 Megahertz
Distance to Tap Point	24 inches

(Each time the program goes through a set of calculations that does not produce a difference of less than 1 percent, the tap point distance goes back through its calculations until the right tap point is found.)

THIS PROGRAM IS DESIGNED TO DETERMINE THE FINAL TAP POINT AND VALUE OF THE SERIES CAPACITOR IN A GAMMA MATCH. THE PROGRAM WILL TAKE THE INITIAL DATA AND GO THROUGH MULTIPLE ITERATIONS UNTIL A SUITABLE MATCH HAS BEEN DETERMINED. THE FINAL TAP POINT WILL BE WITHIN ONE QUARTER OF AN INCH. THIS WILL PROVIDE A SUFFICIENTLY ACCURATE STARTING POINT FOR AN ACTUAL ANTENNA.

ENTER DIAMETER OF ELEMENT? 1

ENTER DIAMETER OF GAMMA ROD? .375

ENTER SPACING BETWEEN ELEMENT AND ROD? 4

ENTER TRANSMISSION SYSTEM IMPEDANCE? 50

ENTER RESISTIVE PORTION OF ANTENNA IMPEDANCE? 35

ENTER REACTIVE PORTION OF ANTENNA IMPEDANCE? -35

ENTER FREQUENCY IN MEGAHERTZ? 16

ENTER DISTANCE IN INCHES FROM CENTER OF DRIVEN ELEMENT TO CENTER OF GAMMA ROD SHORTING

STRAP? 24

 24 INCHES
 21.5639 OHMS

 25 INCHES
 24.0441 OHMS

 26 INCHES
 26.7077 OHMS

27 INCHES 29.5588 OHMS

28 INCHES	32.6002 OHMS
29 INCHES	35.8341 OHMS
30 INCHES	39.2608 OHMS
31 INCHES	42.8794 OHMS
32 INCHES	46.6872 OHMS
32.25 INCHES	47.6684 OHMS
32.5 INCHES	48.6609 OHMS

THE FINAL RESISTANCE IS 49.6648 (A DIFFERENCE OF LESS THAN 1 PERCENT). THE NEW TAP POINT IS AT 32.75 INCHES. THE GAMMA CAPACITOR IS 93.4315 PICOFARADS AGAIN? (1=YES, 0=NO)

?1

ENTER THE PARAMETER YOU WANT TO CHANGE

ELEMENT DIAMETER	1
ROD DIAMETER	2
SPACING	3
SYSTEM IMPEDANCE	4
ANTENNA RESISTANCE	5
ANTENNA REACTANCE	6
FREQUENCY	7

?7
NEW FREQUENCY?
?21
24 INCHES 44.7599 OHMS
THE FINAL RESISTANCE IS 49.9176 (A DIFFERENCE OF
LESS THAN 1 PERCENT). THE NEW TAP POINT IS 25
INCHES. THE GAMMA
CAPACITOR IS 71.0716 PICOFARADS
AGAIN? (1=YES, 0=NO)
? 0
READY

As can be seen in this example, the initial set of information had the tap point on the driven element too close to the center of the element. The program went through the calculations until a suitable tap point was found. Each time through the calculations, the tap point and impedance were displayed to show the progression. Finally, the program reached a point where the increments were changed to 0.25 inch until the final point was reached. Once the correct point was found, the frequency was changed to show

how the same physical conditions could provide a suitable match at a different frequency. As it turns out, at the new frequency of 21 megahertz, only one tap point increment was required. Note the difference between the values for the gamma capacitor.

#### **OMEGA MATCH**

The Omega Match is also a method of matching antennas to transmission lines. In addition to the series capacitor and gamma rod of the Gamma Match, another capacitor is added in parallel across the open end of the Omega rod (see Fig. 4-8). Though a seemingly uncalled for addition to the Gamma Match, the added capacitor allows a person to set the tap point at one spot permanently. Therefore, instead of trying to move the tap point to find the correct matching point, the tap is set at a single spot and the two capacitors are adjusted for a suitable match. Some may deem this an unnecessary complication with little to be gained. However, depending upon the size and installation of the antenna. it may be much easier to settle for the additional capacitor rather than to try to change the gamma rod tap point. This is especially true when the tap point is out greater than three feet from the center of the element. Plus, it is relatively easy to attach a small motor to the capacitors to provide complete, remote tuning capabilities.

The program for the Omega Match is very similar to the previous Gamma Match program. In fact, it is essentially identical up through line 200. At this point, a new factor is added, C. The Omega capacitor, since it is in parallel with the short-circuited transmission line added directly to the reactance presented by this line. The value of C is either incremented or decremented until a suitable match is found.

Electrically, the Omega Match functions essentially as the Gamma Match. For the Omega Match to be effective, though, the tap point must intentionally be set closer to the center of the driven element than would normally be required for a Gamma Match; i.e., if the normal tap point for a Gamma Match was at 25 inches, the

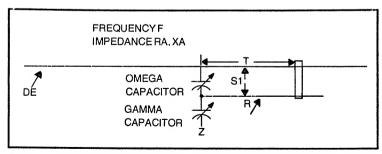


Fig. 4-3. The additional capacities which distinguish the omega match from the gamma match.

Omega Match would require that the point be set less than 25 inches. The closer the tap point is to the correct point for a Gamma Match, the smaller will be the value required for the Omega capacitor. In effect, by setting the tap point closer to the center, you are adding a large amount of inductive reactance due to the short-circuited transmission line effect. By placing the Omega capacitor across the open end of this transmission line you will be able to "tune out" the effects of the transmission line reactance. This essentially allows you to match the antenna via two capacitors.

The formulas used in the Omega Match program are the same as those used for the Gamma Match and won't be repeated.

# Omega Match Program

OMEGA MATCH

```
"TNOHS
                                                                                                                                                                                                                                                                                                                                                                   100 Y=((4*5*5)+(DE42)-(DR42))/(4*5*DE):Y1=L0G(Y+S0R(Y*Y-1))
                                                                                                                                                                              RESISTIVE PORTION OF ANTENNA IMPEDANCE"; RA REACTIVE PORTION OF ANTENNA IMPEDANCE"; XA
                                                                                                                                                                                                                                                                                                                                          90 X=((4*S*S)-(DE+M)+(DK+M))/(4*S*DK):X1=LOG(X+S@K(X*X-1))
                                                                                                                                                                                                                                                          INPUT "ENTER DISTANCE IN INCHES FROM CENTER OF DRIVEN
PRINT"THIS PROGRAM WILL DETERMINE THE VALUES FOR THE
                                                                                                                             SPACING BETWEEN ELEMENT AND ROD" ; S1
                         PRINT"AND SERIES CAPACITORS IN AN OMEGA MATCH."
                                                                                                                                                      TRANSMISSION SYSTEM IMPEDANCE" : Z
                                                                                                                                                                                                                                 FREQUENCY IN MEGAHERTZ" #F
                                                                                                     DIAMETER OF GAMMA ROD" : DR
                                                                            DIAMETER OF ELEMENT"; DE
                                                                                                                                                                                                                                                                                    ELEMENT TO SHORTING STRAP";T
                                                                                                                                                                                                                                                                                                                                                                                             HZ=(1+X1/Y1)+ ⋈
                                                                                                                                                                                                                                                                                                                85 S=DE/2+DR/2+S1
                                                                             "ENTER
                                                                                                                                                                                                                                   "ENTER
                                                                                                       "ENTER
                                                                                                                               "ENTER
                                                                                                                                                        "ENTER
                                                                                                                                                                                "ENTER
                                                                                                                                                                                                           "ENTER
                                                                            INPUT
                                                                                                       INPUT
                                                                                                                               INPUT
                                                                                                                                                        INPUT
                                                                                                                                                                                                           INPUT
                                                                                                                                                                                                                                   INPUT
                                                                                                                                                                                 INPUT
```

ZL1=((4\*5\*5)-(DR42)-(DE42))/(2\*DE\*DR):ZL=60\*(LOG(ZL1+S@R(ZL1\*ZL1-1)) RI=HZ\*RA/(COS(T\*F\*5.32343E-04)) 2:XI=HZ\*XA/(COS(T\*F\*5.32343E-04)) 42

RI(1)=RI:XI(1)=(ZL\*TAN(T\*F\*5.32343E-04))+XI

- RI(2)=ZL-(XI\*TAN(T\*F\*5.32343E-04)):XI(2)=RI\*TAN(T\*F\*5.32343E-04) M1=((RI(1))\*2+(XI(1))E2)\*.5:A1=ATN(XI(1)/RI(1))\*57.2958 M2=((RI(2))\*2+(XI(2))E2)\*.5:A2=ATN(XI(2)/RI(2))\*57.2958
- RR=M3\*COS(A3\*.01745329):XR=(M3\*SIN(A3\*.01745329)) M3=M1/M2:A3=A1-A2
  - RS=RR:XS=XR:C=1
- M4=1/(X8¢2+R8¢2)¢.5:A4=-ATN(XS/RS)\*57.2958
- RP=M4\*COS(A4\*.01745329):XP=M4\*SIN(A4\*.01745329)
- XT=XP+(-1/TAN(T\*F\*5.32343E-04))+(2\*3.1416\*1E-06\*F\*2L\*C) M5=1/(RPC2+XT42)C.5:A5=-ATN(XT/RP)\*57.2958
  - RS(1)=M5\*COS(A5\*.01745329):XS(1)=M5\*SIN(A5\*.01745329) 240
- IF ABS(RF-Z)<Z/100 GOTO 268 ELSE IF RF>Z THEN C=C-1:GOTO 230ELSE RF=ZL\*RS(1):XF=ZL\*XS(1):PRINTRF;"OHMS" 260
  - C=C+1:GOTO 230 IF'C=0 PRINT"THE TAP POINT IS AT THE CORRECT SPOT FOR A GAM MA MATCH. AN OMEGA CAPACITOR IS NOT NECESSARY. THE GAMMA 268
- IF C<0 PRINT"THE TAP POINT IS TOO FAR OUT FOR AN OMEGA MATC CAPACITOR IS";1E6/(2\*3.1416\*F\*XF);"PICOFARADS.":GOTO 352
- PRINT"THE FINAL RESISTANCE IS";RF"(A DIFFERENCE OF LESS N I"CHR\*(13)"PERCENT). THE TAP POINT IS AT";T"INCHES.

H. TRY THE COMPUTATIONS AGAIN WITH ANOTHER TAP POINT. ":GOTO

569

GAMMA CAPACITOR"CHR\*(13)"IS"1E6/(2\*3.1416\*F\*XF);"PICOFARAD THE OMEGA CAPACITOR IS";C;"PICOFARADS."

```
PRINT"ENTER THE PARAMETER YOU WANT TO CHANGE"
                                                                                                                                                                                                                                     SYSTEM IMPEDANCE?":INPUT
                                                                                                                                                                                        ELEMENT DIAMETER?":INPUT
                                                                                                                                                                                                       ROD DIAMETER?":INPUT DR
                                                                                                                                                                                                                     SPACING?":INPUT S1
(1=YES, Ø=NO)":INPUT
                                                                                                          PRINTTAB(10)"ANTENNA RESISTANCE
                                                                                                                           REACTANCE
                                             PRINTTAB(10)"ELEMENT DIAMETER
                                                                                           PRINTTAB(10)"SYSTEM IMPEDANCE
                                                            PRINTTAB(10)"ROD DIAMETER
                                                                                                                                        PRINTTAB(10)"FREQUENCY
                                                                                                                                                        PRINTTAB(10)"TAP POINT
                                                                                                                         PRINTTAB(10)"ANTENNA
                                                                           PRINTTAB(10)"SPACING
                                                                                                                                                                                      PRINT"NEW
                                                                                                                                                                                                     PRINT"NEW
                                                                                                                                                                                                                    PRINT"NEW
                                                                                                                                                                                                                                   PRINT"NEW
                IF G=0 THEN END
PRINT"AGAIN?
                                                                                                                                                                       INPUT N
                                                                                                                                                                                                     NIZ
NIZ
                                                                                                                                                                                        #
#
                                                                                                                                                                                                                   N=3
                                                                                                                                                                                                                                    N=4
                                                            354
                                                                                          356
                                                                                                        357
                                                                                                                                        359
                                                                                                                                                       360
                                                                                                                                                                      361
                                                                                                                                                                                      362
                                                                                                                                                                                                     363
                                                                                                                                                                                                                   364
                                                                                                                                                                                                                                  365
```

ANTENNA RESISTANCE?":INPUT ANTENNA REACTANCE?":INPUT >

FREQUENCY?":INPUT F

PRINT"NEW PRINT"NEW

N=6

PRINT"NEW

366

POINT?":INPUT

TAP

PRINT"NEW

ΩΨ

0109

## **Omega Match Example**

Determine the values for the Omega and Gamma capacitors for an antenna with the following characteristics:

Driven Element Diameter	1 inch
Omega Rod Diameter	.25 inch
Spacing	4 inches
System Impedance	75 ohms
Resistive Part of Antenna Impedance	30 ohms
Reactive Part of Antenna Impedance	$-30\mathrm{ohms}$
Frequency	25 Megahertz
Tap Point Distance	24 inches

THIS PROGRAM WILL DETERMINE THE VALUES FOR THE SHUNT AND SERIES CAPACITORS IN AN OMEGA MATCH.

ENTER DIAMETER OF ELEMENT? 1
ENTER DIAMETER OF GAMMA ROD? .25
ENTER SPACING BETWEEN ELEMENT AND ROD? 4
ENTER TRANSMISSION SYSTEM IMPEDANCE? 75
ENTER RESISTIVE PORTION OF ANTENNA IMPEDANCE?
30
ENTER REACTIVE PORTION OF ANTENNA IMPEDANCE?

ENTER REACTIVE PORTION OF ANTENNA IMPEDANCE? -30

ENTER FREQUENCY IN MEGAHERTZ? 25

ENTER DISTANCE IN INCHES FROM CENTER OF DRIVEN ELEMENT TO SHORTING STRAP? 24

83,3972 OHMS

80.3289 OHMS

77.4027 OHMS

74.6119 OHMS

THE TAP POINT IS TOO FAR OUT FOR AN OMEGA MATCH. TRY THE COMPUTATIONS AGAIN WITH ANOTHER TAP POINT.

## ENTER THE PARAMETER YOU WANT TO CHANGE

ELEMENT DIAMETER	1
ROD DIAMETER	2
SPACING	3
SYSTEM IMPEDANCE	4
ANTENNA RESISTANCE	5
ANTENNA REACTANCE	6
FREQUENCY	7
TAP POINT	8

```
? 8
NEW TAP POINT?
? 22
67.5678 OHMS
70.0705 OHMS
72.6968 OHMS
75.4535 OHMS
THE FINAL RESIS
LESS THAN 1 PER
THE GAMMA CAP
```

THE FINAL RESISTANCE IS 75.4535 (A DIFFERENCE OF LESS THAN 1 PERCENT). THE TAP POINT IS AT 22 INCHES. THE GAMMA CAPACITOR

IS 53.4325 PICOFARADS. THE OMEGA CAPACITOR IS 4 PICOFARADS.

AGAIN? (1=YES, 0=NO)

? 1

## ENTER THE PARAMETER YOU WANT TO CHANGE

ELEMENT DIAMETER	1
ROD DIAMETER	2
SPACING	3
SYSTEM IMPEDANCE	4
ANTENNA RESISTANCE	5
ANTENNA REACTANCE	6
FREQUENCY	7
TAP POINT	8

28

NEW TAP POINT?

? 23

75.3624 OHMS

THE FINAL RESISTANCE IS 75.3624 (A DIFFERENCE OF LESS THAN 1 PERCENT). THE TAP POINT IS AT 23 INCHES. THE GAMMA CAPACITOR

IS 54.0296 PICOFARADS. THE OMEGA CAPACITOR IS 1 PICOFARADS.

AGAIN? (1=YES, 0=NO)

?0

READY

This example was selected to illustrate several features of this Omega Match program. In the first run through the data, the program found that the tap point was too far out from the center of the driven element. This means that the reactive element seen at the open end of the short-circuited transmission line was capacitive rather than inductive. This would have required a variable inductance to act as the compensating element. Next, when the tap point was changed to 22 inches, a suitable match could be found. You'll note that the value for the Omega or parallel capacitor was extremely small. This indicated that the tap point was close to that required for a normal Gamma Match. The last run through the data was with the tap point at 24 inches. This produced a value for the Omega capacitor of 1 picofarad, illustrating the fact that as the tap point gets closer to that required for a Gamma Match, the value of the Omega capacitor gets increasingly smaller. Conversely, as the tap is moved in, the Omega capacitor gets larger.

#### T-PAD

The next three programs deal with three types of attenuators or pads: a T-pad, a Pi-pad, and a minimum loss pad. The T and Pi are named for their characteristic shapes. Each pad will provide a known amount of attenuation after determining the values by using the appropriate program.

Before going into the specifics of the T-pad, I do want to illustrate one useful property of attenuators that is oftentimes overlooked. In addition to providing known amounts of attenuation in a match system, pads can be used to provide impedance matching. Consider Fig. 4-4: this diagram shows a VSWR measuring device connected to some component that exhibits some amount of return loss (VSWR). Return loss is a measure of VSWR; the higher the return loss, the lower the VSWR. A return loss of zero dB is an infinite VSWR. A 1.4:1 VSWR corresponds to a return loss of approximately 15 dB.

In measuring return loss, a small amount of power is applied to the device under test. Some of this power is reflected back to the VSWR measuring device as a function of the VSWR or impedance match. The return loss is the difference, in dB, between the applied and reflected power.

Now, consider Fig. 4-5. In this case the applied power is mostly absorbed by the termination. The difference between applied and reflected power is very large, producing a high return loss. Next look at Fig. 4-6. Now, the 50-ohm load has been replaced with an open circuit. This presents an infinite mismatch, causing all the applied power to be reflected back, producing a return loss of zero dB. Finally, in Fig. 4-7, a 10-dB attenuator has been placed between the VSWR measuring device and the open. The applied power, when passing between the VSWR measuring device and the open, is attenuated 10 dB. At the open, the applied power, now down 10 dB, is reflected back. In the return path back to the VSWR measuring device, the reflected power is also attenuated by 10 dB. Therefore, the difference between the applied and reflected power is 20 dB, twice the value of the pad. Therefore, by simply inserting a 10-dB pad before the open improves the return loss from 0 to 20 dB. This corresponds to a decrease in VSWR from infinitely high to about 1.2:1.

This technique can be applied throughout circuitry to help maintain system and circuit impedance levels. Normally, in today's 50-ohm system, 50-ohm pads are used. However, nothing prevents one from designing pads for different impedance levels.

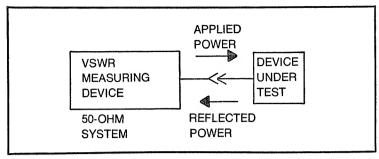


Fig. 4-4. A VSWR measuring device connected to a component which measures return loss.

Another good example is the output of a doubly balanced mixer. For best intermodulation performance, the output of the mixer should see 50-ohms for all frequencies. A pad could be inserted between the mixer and the next device to ensure a good 50-ohm termination at all frequencies. Nothing is free, however. This will only work if the system has enough gain to make up for the loss in the attenuator.

Basically, this is a very simple program. The values for the resistors are computed from the following common-day formulas:

R1 = 
$$Z\left(\frac{10^{.05A} - 1}{10^{.05A} + 1}\right)$$
 R2 =  $\frac{R11Z}{10^{.05A} - 1}$ 

where Z = impedance

A = attenuation value

Once the theoretical values have been determined, the only problem is to obtain these values with practical components. The second part of the program lets you input the real values that will be used and then computes the actual attenuation.

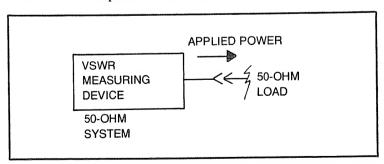


Fig. 4-5. How a VSWR measuring device with a 50 ohm load can absorb applied power.

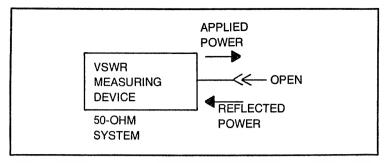


Fig. 4-6. A VSWR measuring device with the 50 ohm load replaced by an open circuit.

## **T-Pad Program**

- 5 'T PAD CALCULATIONS
- 10 CLS
- 20 PRINT"ENTER DESIRED ATTENUATION VALUE"
- 30 INPUT A
- 40 PRINT"ENTER SYSTEM IMPEDANCE"
- 50 INPUT I
- 60 R1=I\*((10 (.05\*A)-1)/(10 (.05\*A)+1))
- 7Ø R2=(R1+I)/(1Ø4(.Ø5\*A)-1)
- 80 PRINT"R1="R1"OHMS", "R2="R2"OHMS
- 90 PRINT"ENTER THE ACTUAL VALUE TO BE USED FOR R1"
- 100 INPUT R1

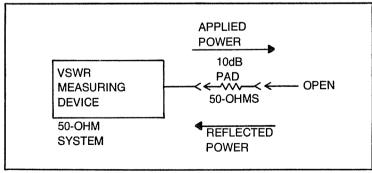


Fig. 4-7. A VSWR measuring device with a 10 dB attenuator placed between the VSWR and the open circuit.

- 110 PRINT"ENTER THE ACTUAL VALUE TO BE USED FOR R2"
- 120 INPUT R2
- 130 Z = (R2\*(I+R1))/(R1+R2+I)+R1
- 140 PRINT"WITH ONE SIDE ACTUALLY T ERMINATED IN"I"OHMS, THE OPPOS ITE"CHR\$(13)"SIDE OF THE PAD W ILL APPEAR AS"Z"OHMS."
- 15Ø E=R2/(I+R1+R2)
- 160 DB=20\*(LOG(1/E)/LOG(10))
- 165 PRINT
- 170 PRINT"WITH R1 = "R1"OHMS AND R2 = "R2"OHMS, THE ACTUAL ATTENUA TION"CHR\$(13)"IS"DB"DB."

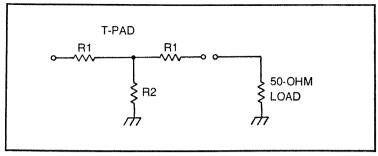


Fig. 4-8. The component designations for a 50 ohm pad with 17 dB of attenuation.

## **T-Pad Examples**

You need a 50-ohm pad with 17 dB of attenuation. What are the required values? (See Fig. 4-8 for the component designations.) ENTER DESIRED ATTENUATION VALUE

? 17

**ENTER SYSTEM IMPEDANCE** 

2.50

R1 = 37.6229 OHMS R2 = 14.413 OHMS

ENTER THE ACTUAL VALUE TO BE USED FOR R1 ? 39

ENTER THE ACTUAL VALUE TO BE USED FOR R2? 10

WITH ONE SIDE ACTUALLY TERMINATED IN 50 OHMS, THE OPPOSITE SIDE OF THE PAD WILL APPEAR AS 47.9899 OHMS.

WITH R1 = 39 OHMS AND R2 = 10 OHMS, THE ACTUAL ATTENUATION IS 19.9127 DB.

This example readily illustrates the usefulness of this program. Since the required resistors are not of normal value, practical components have been substituted to build the T-pad. In this example, using real-world components have changed the attenuation almost 3 dB. It would be better to use a 15-ohm resistor in place of the 10-ohm resistor. This would decrease the actual attenuation to 16.8 dB vs 19.9. The impedance would also change, actually getting closer to 50 ohms.

#### PI-PAD

The next program covers the Pi-pad. This program is very similar to the previous T-pad program, providing the computed values and then allowing for real-world components. The best approach would be to determine the desired attenuation value and then to run both programs. From this dual information you can then select the best pad according to the components on hand.

The equations used for determination of the resistor values in the Pi-pad are:

$$R1 = Z \left( \frac{10^{.05A} + 1}{10^{.05A} - 1} \right) R2 = \frac{Z R1 (10^{.05A} - 1)}{Z + R1}$$

## Sample Pi-pad Program

- 5 'PI PAD
- 10 CLS
- 20 PRINT"ENTER DESIRED ATTENUATION VALUE
- 30 INPUT A
- 40 PRINT"ENTER SYSTEM IMPEDANCE"
- 50 INPUT Z
- 6Ø R1=Z\*(1Ø\*(.Ø5\*A)+1)/(1Ø\*(.Ø5\*A) -1)
- 70 R2=Z\*R1\*(10) (.05\*A)-1)/(Z+R1)
- 80 PRINT"THE REQUIRED RESISTOR FOR R1 IS"R1"OHMS, WHILE R2 SHOULD BE"R2"OHMS
- 90 PRINT"ENTER THE ACTUAL VALUE TO BE USED FOR R1"
- 100 INPUT RN1
- 110 PRINT"ENTER THE ACTUAL VALUE T BE USED FOR R2"
- 120 INPUT RN2
- 13Ø RI=(Z\*(RN1+RN2)+(RN1\*RN2))/(Z+RN1)
- 14Ø RT=R1\*RI/(RI+R1)
- 150 PRINT"WITH ONE SIDE ACTUALLY T ERMINATED IN"Z"OHMS, THE OPPOS SIDE WILL APPEAR AS"RT"OHMS
- 160 E=Z\*RN1/(RI\*Z+RI\*RN1)

170 EF=-20\*(LOG(E)/LOG(10))
180 PRINT"THE ACTUAL ATTENUATION W
ILL BE"EF"DB.

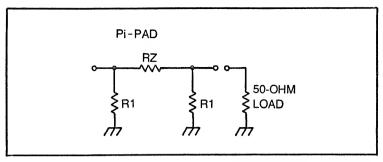


Fig. 4-9. Resistor designations required to determine the value of resistors needed for a 12 dB pad on a 600 ohm system.

## Sample Pi-pad Program

What value resistors are required to make a 12-dB pad for a 600-ohm system? See Fig. 4-9 for the resistor designations.

ENTER DESIRED ATTENUATION VALUE

? 12

**ENTER SYSTEM IMPEDANCE** 

? 600

R1 = 1118.97

R2 = 1002.54

ENTER THE ACTUAL VALUE TO BE USED FOR R1

? 1200

ENTER THE ACTUAL VALUE TO BE USED FOR R2 ? 1000

WITH ONE SIDE ACTUALLY TERMINATED IN 600 OHMS, THE OPPOSITE SIDE OF THE PAD WILL APPEAR AS 612.6 OHMS.

WITH R1 = 1200 OHMS AND R2 = 1000 OHMS, THE ACTUAL ATTENUATION IS 12 DB.

You can see from this example that as the system impedance goes higher, the pad becomes more tolerant to resistance values.

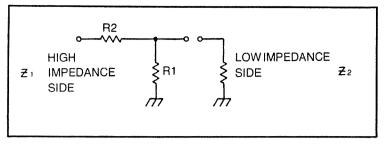


Fig. 4-10. Values for 2 resistors and their loss through the pad.

#### MINIMUM-LOSS PAD

The last attenuator program is a special case known as a minimum-loss pad. The pad is characterized by the ability to match impedances, whereas the T- and Pi-pad are able to swamp out impedance mismatches. However, the minimum-loss pad is also characterized by a high impedance loss through the pad. If the high loss can be tolerated, this is one excellent way of matching between two circuits. The program will provide the values for the two resistors (see Fig. 4-10 for the component designations) and the loss through the pad. The only other stipulation is that the pad is not bi-directional; it can only be installed in the circuit in one way.

The equations to determine the component values for the minimum loss pad are:

$$R1 = Z_1 (1 - Z_9/Z_1)^{1/2}$$
  $R2 = Z_9/(1 - (Z_9/Z_1))^{1/2}$ 

# **Minimum Loss Pad Program**

5 'MINIMUM LOSS PAD

10 CLS

20 PRINT "ENTER THE IMPEDANCES TO
BE MATCHED (HIGH, LOW)

30 INPUT Z(1),Z(2)

40 R(1)=Z(1)\*SQR(1-Z(2)/Z(1))

50 R(2)=Z(2)/SQR(1-Z(2)/Z(1))

60 PRINT"R1="R(1)"OHMS"

70 PRINT"R2="R(2)"OHMS"

80 L=LOG((Z(1)-R(1))/Z(1))/LOG(10)

90 PRINT"THE LOSS IS "20\*L"DB"

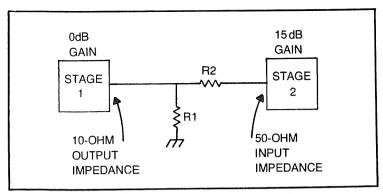


Fig. 4-11. Matching a 10 ohm output to a 50 ohm input.

## **Example Minimum Loss Program**

As seen in Fig. 4-11, you wish to match the 10-ohm output of the first stage to the 50-ohm input of the second stage which is an rf amplifier. The amplifier has 15-dB gain. What are the values of the matching resistors and overall gain from the input of the first stage to the output of the second stage?

ENTER THE IMPEDANCES TO BE MATCHED (HIGH, LOW) ? 50.10

R1 = 44.7214 OHMS

R2 = 11.1803 OHMS

THE LOSS IS - 19.529 DB.

Overall gain, therefore, is  $-4.5 \, dB$ .

#### PARALLEL/SERIES CONVERSIONS

As mentioned in the section of the Gamma Match program, parallel/series conversions are used during impedance transformations. There are two methods of presenting impedance data: series format and parallel format. In both cases, they consist of a real, resistive component in either series or parallel, with an imaginary, reactive component. Though the values are different, the overall impedance is still the same since this is just two different ways of presenting the same data. Generally, most information is presented in series format. However, in some cases, as in particular when paralleling components, it is easier to work with the data in a parallel format. In this way values can be added directly.

One area where this parallel presentation of impedance information is prevelant is the output of rf power transistors. In many cases manufacturers will present the transistor's input characteristics in series form and the output characteristics in a parallel form.

The equations for series/parallel conversion are:

$$R_{s} = \frac{R_{p}}{1 + \left(\frac{R_{p}}{X_{p}}\right)}$$

$$X_{s} = R_{s} \left(\frac{R_{p}}{X_{p}}\right)$$

$$R_{p} = R_{s} (1 + (X_{s}/R_{s})^{2})$$

$$X_{p} = \frac{R_{p}}{X_{s}/R_{s}}$$

Note that when using the plus and minus signs for the reactances they will carry through the equations to give the correct sign for the answer.

# Parallel/Series Program

```
5 ' TO S AND S TO P CONVERSION
10 CLS
20 PRINT"ENTER ""S"" IF CONVERSION
IS PARALLEL TO SERIES OR ""P""
```

- IF"CHR\$(13)"CONVERSION IS SERIES TO PARALLEL"
- 30 INPUT C\$
- 40 IF C\$="P"GOTO 130
- 50 PRINT"ENTER THE PARALLEL RESIST ANCE, RP (OHMS)"
- **60 INPUT RP**
- 70 PRINT"ENTER THE PARALLEL REACTA NCE, XP (OHMS)"
- 80 INPUT XP
- 90 RS=RP/(1+(RP/XP) ↑2)
- 100 XS=RS\*RP/XP
- 110 PRINT"THE SERIES RESISTIVE PAR T IS"RS"OHMS AND THE SERIES"CH R\$(13)"REACTIVE IS"XS"OHMS
- 120 END
- 130 PRINT"ENTER THE SERIES RESISTA NCE, RS (OHMS)"
- 140 INPUT RS
- 150 PRINT"ENTER THE SERIES REACTAN

  CE, XS (OHMS)"
- 160 INPUT XS
- 170 RP=RS\*(1+(XS/RS))2)
- 18Ø XP=RP/(XS/RS)
- 190 PRINT"THE PARALLEL RESISTIVE P ART IS"RP"OHMS AND THE PARALLE L"CHR\$(13)"REACTIVE PART IS"XP "OHMS

# Parallel/Series Examples

The optimum source impedance for best noise figure of a microwave transistor is 12.5 +j0.5 ohms. What is this same impedance expressed as a parallel equivalent?

ENTER S IF CONVERSION IS PARALLEL TO SERIES OR P IF CONVERSION IS SERIES TO PARALLEL

? P

ENTER THE SERIES RESISTANCE, RS (OHMS)

? 12.5

ENTER THE SERIES REACTANCE, XS (OHMS)

?.5

THE PARALLEL RESISTIVE PART IS 12.52 OHMS AND THE PARALLEL

REACTIVE PART IS 313 OHMS

Express 80-j90 ohms as a series equivalent.

ENTER S IF CONVERSION IS PARALLEL TO SERIES OR P IF CONVERSION IS SERIES TO PARALLEL

? S

ENTER THE PARALLEL RESISTANCE, RP (OHMS)

?80

ENTER THE PARALLEL REACTANCE, XP (OHMS)

? - 90

THE SERIES RESISTIVE PART IS 44.6897 OHMS AND THE SERIES

REACTIVE PART IS -39.7241 OHMS

## MATCHING NETWORKS

The four programs to follow will solve for the required reactive values in the following impedance matching networks. Since the answers are given in reactive values, they can be scaled to any frequency by using the appropriate reactance formula and frequency. The first program is for network A which is shown in Fig. 4-12.

This network is only used when the device that is to be matched has a series real part less than the load impedance. If you were to run this program several times you would see that as the real part approaches the load impedance, the reactance of C1 increases toward infinity. This network, though, can be used for RF power transistor design since their input and output impedances are generally very small.

The equations to solve network A are:

$$XL = QR + X_{C}$$

$$XC2 = AR_{L}$$

$$XC1 = \frac{(B/A)(B/Q)}{(B/A) - (B/Q)} = \frac{B}{Q - A}$$
where  $A = \sqrt{\left(\frac{R(1 + Q^{2})}{R_{L}}\right)} - 1$ 

$$B = R(1 + Q^{2})$$

## **Network A Program**

5 'MATCHING NETWORK A 10 CLS 20 PRINT"SELECT A VALUE FOR Q"

30 INPUT Q

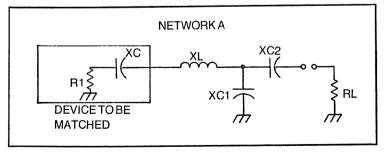


Fig. 4-12. Network A, for which Program 4-8 is designed.

- 40 PRINT"ENTER THE LOAD IMPEDANCE"
- 50 INPUT RL
- 60 PRINT"WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENT ER"CHR\$(13)"THE RESISTIVE (OHMS). AND REACTIVE ELEMENTS (OHMS).
- 70 INPUT RIXC
- 80 M=SQR((R\*(1+Q $\neq$ 2)/RL)-1)
- 90 N=R\*(1+G\*2)
- $100 \times R + XC$
- 110 XC(1)=N/(Q-M)
- 12Ø XC(2)=M\*RL
- 130 PRINT"XL="XL(1)"OHMS"
- 140 PRINT"XC1="XC(1)"OHMS"
- 150 PRINT"XC2="XC(2)"OHMS"

## **Network A Example**

Using the diagram shown in Fig. 4-13, determine the reactance values for the matching components.

SELECT A VALUE FOR Q

?3

ENTER THE LOAD IMPEDANCE

? 75

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

?20, -30

XL = 30 OHMS

XC1 = 117.027 OHMS

XC2 = 96.8246 OHMS

READY

You'll notice that, in this example, the reactance of the inductor matches the reactance of the output capacitance. In this way, the reactive element is cancelled and the two capacitors transform the real part of the output impedance up to the 75-ohm load impedance.

To illustrate the problem encountered with a series real part close the load impedance, run the following information: Q = 3, ZL = 75. Real Part = 74, and Imaginary Part = -30

SELECT A VALUE FOR Q

?3

ENTER THE LOAD IMPEDANCE

? 75

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

?74. -30

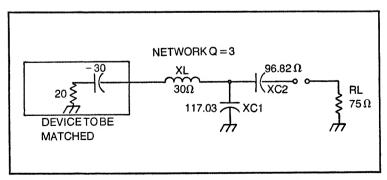


Fig. 4-13. Network Q-3, to be used in Network A problem.

XL = 192 OHMS

XC1 = 33177.5 OHMS

XC2 = 223.327 OHMS

When applied to the standard capacitive reactance formula, the 33000+ ohms create a very small capacitor value.

## **Network B Example**

Network B, as shown in Fig. 4-14 is the Pi network which has been widely used to match the output of a vacuum-tube transmitter to a transmission line.

The main limitation of this network deals with the selection of Q and the matching range. When a low Q is selected, the value of the parallel real part of the output impedance must also be low. This will be illustrated in the following examples. Notice that the program calls for the data to be input in a series equivalent format. If you wish to use the series format, delete line 71. Otherwise, leave line 71 in and input the data in a parallel format. The type of format you use will depend generally upon the device being matched. For example, some power transmitters present their output impedance data in a parallel equivalent, while others use a series equivalent format. Power tubes, on the other hand, use a parallel format.

The equations to solve for the required component values are:

## **Network B Program**

5 'MATCHING NETWORK B 10 CLS 20 PRINT"SELECT A VALUE FOR Q"

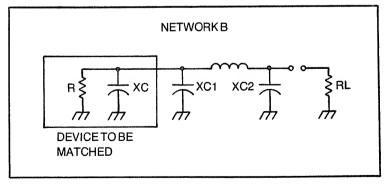


Fig. 4-14. Network B, for which Program 4-9 is designed.

- 30 INPUT Q
- 40 PRINT"ENTER THE LOAD IMPEDANCE"
- 50 INPUT RL
- 60 PRINT"WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENT ER"CHR\$(13)"THE RESISTIVE (OHMS).

  AND REACTIVE ELEMENTS (OHMS).
- 70 INPUT R,XC
- 71 RP=R:XP=XC:GOTO 100
- 80 RP=R\*(1+(XC/R) 12)
- 90 XP=RP/(XC/R)
- 100 XC(1)=RP/0
- 110 XC(2)=RL\*SQR((RP/RL)/((Q\*2+1)-(RP/RL)))
- 12Ø XL=(@\*RP+(RP\*RL/XC(2)))/(@+2+1)
- 130 PRINT"XC1="XC(1)"OHMS"
- 140 PRINT"XC2="XC(2)"OHMS"
- 15Ø PRINT"XL="XL"OHMS"

## Sample Network B Problems

Match the output of the vacuum tube transmitter shown in Fig. 4-15 using a network with a Q of 5 and a load impedance of 50 ohms. (Since the diagram shows the output in a parallel format, leave line 71 in the program.)

SELECT A VALUE FOR Q

?5

ENTER THE LOAD IMPEDANCE

? 50

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

? 2000, 10

?FC ERROR IN 110

This example shows that with the high real part of the impedance to be matched and with the low Q of the network, there is no solution to the problem. To achieve a solution, the circuit Q will have to be raised.

SELECT A VALUE FOR Q

? 15

ENTER THE LOAD IMPEDANCE

? 50

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

?2000, 10

XC1 = 133.333 OHMS

XC2 = 23.1869 OHMS

XL = 151.826 OHMS

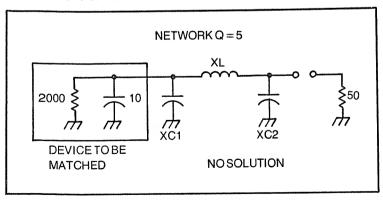


Fig. 4-15. Network Q-5, to be used in Network B problem.

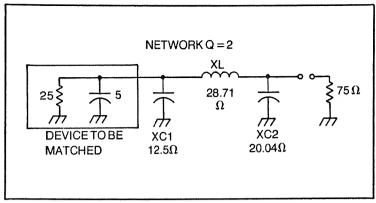


Fig. 4-16. Network Q-2, to be used in Network B problem.

In actual practice, the value for C1 = C1 - Output C. Depending upon the frequency and the matching components, C1 can actually be eliminated and the output capacitance of the tube will suffice for the matching capacitor. This, generally, happens only at frequencies greater than 40 to 50 megahertz.

Match the output impedance of the circuit shown in Fig. 4-16 to 50 ohms using a network with a Q of 2.

SELECT A VALUE FOR Q

?2

ENTER THE LOAD IMPEDANCE

? 75

WITH THE IMPEDANCE TO BE MATCHING IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

? 25.5

XC1 = 12.5 OHMS

XC2 = 20.0446 OHMS

XL = 28.7083 OHMS

### **Network C**

Network C can be implemented by either of the two methods shown in Fig. 4-17.

This program, though, is designed to solve for the matching network when the data is presented in a series equivalent format. In either case, the real part of the impedance to be matched must be less than the load impedance. Practically, this configuration yields the best component values when the real part is of a low value.

The equations to solve network C are:

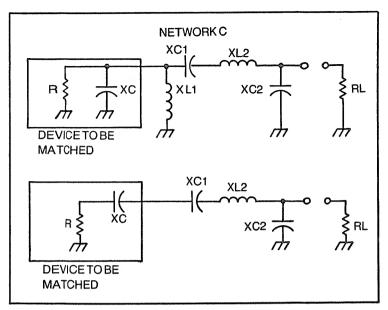


Fig. 4-17. Two methods by which Network C can be implemented.

XL1=XC  
XC1=QR  
XC2=RL 
$$\sqrt{\frac{R1}{RL-R}}$$
  
XL2=XC1+ $\left(\frac{RRL}{XC2}\right)$ 

Parallel Format

$$XC1 = QR1$$

$$XC2 = RL \sqrt{\frac{R}{RL - R}}$$

$$XL2 = XC1 + \left(\frac{RRL}{XC2}\right) + XC$$

Series Format

# **Network C Program**

5 'MATCHING NETWORK C

10 CLS

20 PRINT"SELECT A VALUE FOR Q"

- 30 INPUT @
- 40 PRINT"ENTER THE LOAD IMPEDANCE"
- 50 INPUT RL
- 60 PRINT"WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENT ER"CHR\$(13)"THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).
- 70 INPUT RIXC
- $100 \times C(1) = R \times Q$
- 110 XC(2)=RL\*SQR(R/(RL-R))
- 120 XL(1) = XC(1) + (R\*RL/XC(2)) + XC
- 130 PRINT"XL="XL(1)"OHMS"
- 140 PRINT"XC1="XC(1)"0HMS"
- 150 PRINT"XC2="XC(2)"0HMS"

## Sample Network C Programs

Match the circuit shown in Fig. 4-18 using Network C with a  ${\bf Q}$  of 5.

SELECT A VALUE FOR Q

23

ENTER THE LOAD IMPEDANCE

? 50

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

? 60,300

? FC ERROR IN 110

READY

This illustrates the point that the load impedance must be higher than the series real part. Now, try solving the network by raising the load impedance to 75 ohms

SELECT A VALUE FOR Q

?3

ENTER THE LOAD IMPEDANCE

? 75

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

? 60.300

XL = 510 OHMS

XC1 = 180 OHMS

XC2 = 150 OHMS

READY

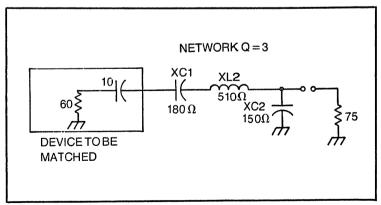


Fig. 4-18. Network Q-3, to be used in Network C problem.

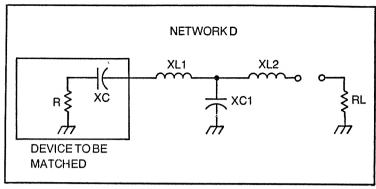


Fig. 4-19. Network D.

#### **Network D**

The last program covers Network D, the classical T type of network. An illustration of Network D is given in Fig. 4-19. The advantage of this network is that it will match load impedances that are both less than and greater than the series real part of the impedance to be matched.

Equations to use this network are:

$$XL1 = RQ + XC$$

$$XL2 = RLB$$

$$XC1 = \frac{A}{Q+B}$$
where  $A = R(1+Q^2)$ 

$$B = \sqrt{\frac{A}{RL} - 1}$$

# **Network D Program**

- 5 'MATCHING NETWORK D
- 10 CLS
- 20 PRINT"SELECT A VALUE FOR Q"
- 30 INPUT Q
- 40 PRINT"ENTER THE LOAD IMPEDANCE"
- 50 INPUT RL
- 60 PRINT"WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENT ER"CHR\$(13)"THE RESISTIVE (OHMS).

70 INPUT R;XC
80 M=R\*(1+0\*2)
90 N=SQR(M/RL-1)
100 XL(1)=R\*Q+XC
110 XL(2)=RL\*N
120 XC=M/(Q+N)
130 PRINT"XL1="XL(1)"OHMS"
140 PRINT"XL2="XL(2)"OHMS"
150 PRINT"XC="XC"OHMS"

## Sample Network D Problems

Match the circuit shown in Fig. 4-20A by using network D. The load impedance is 50 ohms and the circuit Q is 10.

SELECT A VALUE FOR Q

? 10

ENTER THE LOAD IMPEDANCE

? 50

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE (OHMS) ELEMENTS.

? 5.10

XL1 = 60 OHMS

XL2 = 150.831 OHMS

XC = 38.7966 OHMS

Match the circuit shown in Fig. 4-20B to a load impedance of 50 ohms using network D with a circuit Q of 10.

SELECT A VALUE FOR Q

? 10

ENTER THE LOAD IMPEDANCE

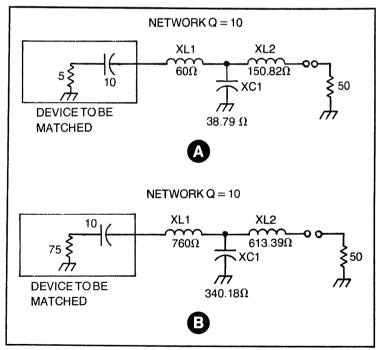


Fig. 4-20. Network Q-10, to be used in Network D problem.

? 50

WITH THE IMPEDANCE TO BE MATCHED IN A SERIES FORMAT, ENTER THE RESISTIVE (OHMS) AND REACTIVE ELEMENTS (OHMS).

? 75.10

XL1 = 760 OHMS

XL2 = 613.392 OHMS

XC = 340.177 OHMS

This illustrates that, regardless of the value of the series real part, the T network is able to perform the necessary matching.

#### CAPACITIVE-DIVIDER NETWORK

The last network to be discussed is the capacitive-divider transformer. This network uses a resonant circuit to match between a low and high impedance. Whereas the minimum loss pad had considerable loss, this circuit exhibits only minimal loss. In addition, since a tuned circuit is used, it shows a band pass characteristic and is therefore useful in minimizing harmonic energy. Since specific frequencies are used for the center frequency and bandwidth, the solution provided by this program is a listing of real component values rather than reactances.

To solve the capacitive-divider transformer manually, use the following equations and Fig. 4-21:

$$Q = \frac{\text{Center Freq.}}{\text{Bandwidth}}$$

$$CT = \frac{Q}{2\pi 1 = \left(\frac{\text{RL}}{2}\right)} \times 10^{6}$$

$$C2/C1 = \sqrt{\frac{\text{RL}}{R}} - 1$$

$$CT = \frac{C1 \times C2}{C1 + C2}$$

# Capacitive-Divider Network Program

- 5 'CAPACITIVE DIVIDER TRANSFORMER
- 10 CLS
- 20 PRINT"ENTER LOAD IMPEDANCE (>50 OHMS)"
- 30 INPUT RL
- 40 PRINT"ENTER CENTER FREQUENCY (M HZ)"

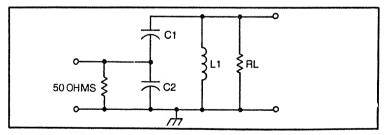


Fig. 4-21. A C-D Transformer.

- 50 INPUT F
- **60 PRINT"ENTER BANDWIDTH (MHZ)"**
- 70 INPUT B
- 80 Q=F/B
- 90 CT=@\*1E6/(2\*3.1416\*F\*(RL/2))
- 100 M = SQR(RL/50) 1
- 11Ø C1=CT/(M/(M+1))
- 120 C2=M\*C1
- 13Ø L=1/(4\*3.1416\*2\*F\*2\*CT\*1E-6)
- 150 PRINT"C1="C1"PICOFARADS"
- 160 PRINT"C2="C2"PICOFARADS"
- 170 PRINT" L="L"MICROHENRYS"

## **Example Capacitive-Divider Network Problem**

Using the capacitive-divider transformer network shown in Fig. 4-22, determine the required component values for a bandwidth of 250 kHz at a center frequency of 10 MHz.

ENTER LOAD IMPEDANCE (>50 OHMS)

? 500

ENTER CENTER FREQUENCY (MHZ)

? 10

ENTER BANDWIDTH (MHZ)

?.250

C1 = 3724.15 PICOFARADS

C2 = 8052.66 PICOFARADS

L = .0994715 MICROHENRYS

As proof, determine the resonant frequency of the tuned circuit by:

$$f = \frac{1}{2\pi\sqrt{LC}}$$

where C = series capacitance of C1 and C2

$$f = \frac{1}{\sqrt{2\pi \cdot .099 \times 10^{-6} \cdot 2.55 \times 10^{-9}}}$$

$$f = \frac{.159}{\sqrt{2.52 \times 10^{-16}}} = \frac{.159}{1.59 \times 10^{-8}} = 10.01 \text{ MHz}$$

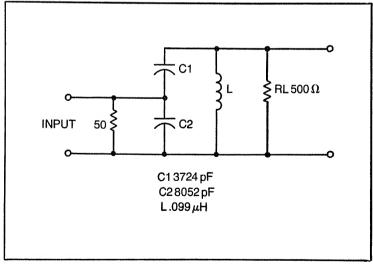


Fig. 4-22. C-D transformer network to be used in example problem.

#### SERIES-MATCHING SECTION

This next program uses a rather unusual matching technique known as the series-matching section. Because of the materials involved, it is more applicable to matching antennas rather than circuits. This technique uses a group of different impedance transmission lines matching different impedances. To understand, see Fig. 4-23; this diagram illustrates that two different impedance sections of transmission line are inserted between the system transmission line and the load to be matched.

The program computes the lengths of the matching sections in electrical degrees. For practical implementation, the velocity factor constant will have to be applied to find the physical lengths. Using real transmission lines the different impedance values that can be matched are somewhat limited, however, there is enough range to match most real-world type of requirements. At higher frequencies where stripline and microstrip construction are prevalent, the impedance of the transmission line can be tailored to fit the needs of the matching problem.

The equations used to determine the length of the matching sections are:

$$L2 = \tan^{-1} \sqrt{\frac{(R-1)^2 + X^2}{R(N - \frac{1}{N})^2 (R-1)^2 - X^2}} = B$$

L1 = 
$$\tan^{-1} \frac{(N - \frac{R}{N} B + X)}{R + XNB - 1} = A$$

where 
$$N = \frac{Z \text{ match}}{Z \text{ line}}$$

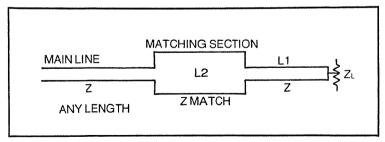


Fig. 4-23. A series-matching section illustrating two difference impedance sections of transmission line.

$$R = \frac{RL}{Z_o}$$

$$X = \frac{XL}{Z_0}$$

In some cases, the values of impedance for the matching section and main line section are too close together. This may cause the quantity under the radical to be negative, an invalid solution. The limits on the impedance of the transmission line can be calculated by the following formulas:

$$Z_{\text{match}} > Z_{\text{line}} \sqrt{\text{SWR}} \text{ or } Z_{\text{match}} < Z_{\text{line}} \sqrt{\text{SWR}}$$
FOR MATCHING TO OCCUR

The program automatically calculates these limits and gives an error message when the values are too close.

#### **Series Section Program**

```
5 'SERIES MATCHING SECTION
10 CLS
20 PRINT"ENTER LOAD IMPEDANCE (R:X
   )
30 INPUT R,X
40 PRINT"ENTER THE IMPEDANCE OF TH
   E MAIN LINE"
5Ø INPUT Z(1)
60 PRINT"ENTER THE IMPEDANCE OF TH
   E MATCHING SECTION"
70 INPUT Z(2)
71 S=SQR(R\neq2+X\neq2)/Z(1)
72 IF S<1 THEN S=1/S
75 GOTO 110
80 N=Z(2)/Z(1)
90 R=R/Z(1)
100 X = X/Z(1)
1Ø5 GOTO 125
110 IF Z(2) > Z(1) * SQR(S) OR Z(2) < Z(
    1)/SQR(S)GOTO 120 ELSE PRINT"I
    NSUFFICIENT RANGE FOR MATCHINGI
       CHOOSE A NEW VALUE FOR THE"
    CHR$(13)"MATCHING SECTION"
```

- 115 GOTO 20
- 120 GOTO 80
- 125 ON ERROR GOTO 190
- 13Ø B=SQR((((R-1)\*2+(X\*2))/(R\*(N-1/ N)\*2-(R-1)\*2-(X\*2)))
- 140 A = ((N-R/N)\*B+X)/(R+X\*B\*N-1)
- 150 IF ATN(A)\*57.29578<0 THEN L1=A TN(A)\*57.29578+180 ELSE L1=ATN (A)\*57.29578
- 160 L2=ATN(B)\*57.29578
- 170 PRINT"SECTION 1 -- "L1"DEGREES"
- 180 PRINT"SECTION 2 -- "L2" DEGREES"
- 185 END
- 190 PRINT"INSUFFICIENT RANGE FOR M ATCHING. CHOOSE A NEW VALUE F OR"CHR\$(13)"THE MATCHING SECTI ON.":GOTO 60

## **Series Matching Section Examples**

Match the antenna shown in Fig. 4-24 with a series matching section to a 50-ohm transmission line. The impedance of the matching section is 75 ohms.

ENTER LOAD IMPEDANCE (R.X)

? 250, 100

ENTER THE IMPEDANCE OF THE MAIN LINE

?50

ENTER THE IMPEDANCE OF THE MATCHING SECTION ? 75

INSUFFICIENT RANGE FOR MATCHING. CHOOSE A NEW VALUE FOR THE MATCHING SECTION

ENTER LOAD IMPEDANCE (R,X)

? 250, 100

ENTER THE IMPEDANCE OF THE MATCHING SECTION ? 93

INSUFFICIENT RANGE FOR MATCHING. CHOOSE A NEW VALUE FOR THE MATCHING SECTION.

ENTER LOAD IMPEDANCE (R,X)

? 250.100

ENTER THE IMPEDANCE OF THE MAIN LINE

? 50

ENTER THE IMPEDANCE OF THE MATCHING SECTION ? 300

SECTION 1 — 24.8774 DEGREES

SECTION 2 — 20.051 DEGREES

This example shows that you would have to use a section of 300-ohm balanced line to match the load. This might present some practical problems, interfacing between the 50-ohm unbalanced and 300-ohm balanced lines. However, it illustrates the wide range of antenna matching that can be achieved by using the seriesmatching section.

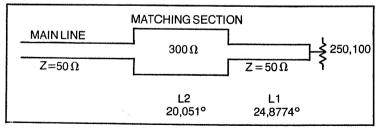


Fig. 4-24. Antenna to be used in solving the series-matching section problem.

#### **MICROSTRIP**

The last program in this chapter is used to determine the width of microstrip transmission lines for specific values of impedance. As I mentioned in the previous section, the microstrip transmission lines can be tailored in impedance to fulfill the matching requirements. In many other cases, the impedance of the microstrip is also tailored to meet the matching requirements, i.e., low noise microwave amplifiers or vhf/uhf power amplifiers.

Figure 4-25 illustrates the relationships that are used in this program. The microstrip is that portion of the copper cladding that is not etched away. To compute the width of the microstrip, two different formulas are used. Once the width is determined, the correct answer is chosen according to the width-to-height ratio. Lines 60 through 90 perform the actual computations for the two formulas, while line 180 determines which answer of the two to use.

The two formulas to calculate the width of the microstrip are:

$$w/h < 2 \qquad w/h = \frac{8^{e^A}}{e^{2A} - 2}$$
 
$$w/h > 2 \qquad w/h = \frac{2}{\pi} (B - 1 - (n(2B - 1) + \frac{E_r - 1}{Z_{E_r}})$$
 
$$(1n(B - 1) + .39 - \frac{.61}{E_r})$$

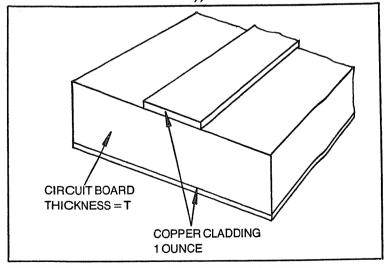


Fig. 4-25. The relationships used in the microstrip program.

where A = 
$$\frac{Z_o}{60}\sqrt{\frac{E_r + 1}{2}} + \frac{E_r - 1}{E_r + 1}(.23 + \frac{.11}{E_r})$$
  
B =  $\frac{377 \pi}{2Z \sqrt{E}}$ 

## **Microstrip Program**

- 5 'MICROSTRIP CALCULATIONS
- 10 CLS
- 20 PRINT"ENTER DESIRED IMPEDANCE OF MICROSTRIP"
- 30 INPUT Z
- 40 PRINT"ENTER DIELECTRIC CONSTANT OF CIRCUIT BOARD MATERIAL"
- 50 INPUT E
- 55 GOTO 100
- 60 A=(Z/60)\*SQR((E+1)/2)+((E-1)/(E+1))\*(.11/E+.23)
- 70 B=592.1902/(Z\*SQR(E))
- 80 WH(1)=8\*2.7183\*A/(2.7183\*(2\*A)-2)
- 90 WH(2)=.6366\*((B-1)-LOG(2\*B-1)+( (E-1)/(2\*E))\*(LOG(B-1)+.39-.61/ E))
- 95 GOTO 140
- 100 PRINT"ENTER THICKNESS OF CIRCU IT BOARD (MILS)
- 110 INPUT T
- 120 PRINT"ENTER THICKNESS OF COPPE R (OUNCES)
- 130 INPUT O
- 135 GOTO 60
- $140 0 = 0 \times 1.4$
- 150 H=T-2\*0
- 160 R=WH(1)\*H
- 170 S=WH(2)\*H
- 180 IF WH(1)<2 PRINT"THE MICROSTRI P IS"R"MILS WIDE" ELSE PRINT"T HE MICROSTRIP IS"S"MILS WIDE"

#### Microstrip Examples

Determine the width of a 50-ohm line on a glass epoxy board that is 1/16-inch thick. The copper clad is 1 ounce.

ENTER DESIRED IMPEDANCE OF MICROSTRIP

? 50

ENTER DIELECTRIC CONSTANT OF CIRCUIT BOARD MATERIAL

? 5 (Glass epoxy)

ENTER THICKNESS OF CIRCUIT BOARD (MILS)

? 62

ENTER THICKNESS OF COPPER (OUNCES)

?1

THE MICROSTRIP IS 102.721 MILS WIDE.

Next, compute the width of the same microstrip except on an alumina substrate.

ENTER DESIRED IMPEDANCE OF MICROSTRIP

? 50

ENTER DIELECTRIC CONSTANT OF CIRCUIT BOARD MATERIAL

28.8

ENTER THICKNESS OF CIRCUIT BOARD (MILS)

? 62

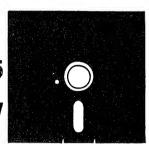
ENTER THICKNESS OF COPPER (OUNCES)

?1

THE MICROSTRIP IS 63.8949 MILS WIDE.

This illustrates that as the dielectric constant of the circuit board material is raised, the lines can be of smaller width. By using substrates with a higher dielectric constant, microwave circuitry can be reduced significantly in size as compared to lower frequency type of circuits.

# Chapter 5 Geometry



This last chapter is not a return to the eighth grade. However, it is devoted to the person who uses his computer for the more exotic problems. The first group of programs in this chapter will deal with the hyperbolic functions which are used in a lot of engineering problems. In addition, hyperbolic functions are quite useful in connection with differential equations.

### HYPERBOLIC FUNCTIONS

The basic identities of the hyperboic sine and cosine are related to the coordinates of the points X, Y on the basic hyperbola  $X^2 - Y^2 = 1$ . Sinh and Cosh, the hyperboic sine and cosine, respectively, are identified as follows:

Sinh X = 
$$\frac{1}{2}$$
 (e<sup>x</sup> - e<sup>-x</sup>)  
Cosh X =  $\frac{1}{2}$  (e<sup>x</sup> + e<sup>-x</sup>)

The remaining hyperbolic functions are defined in terms of sinh x and cosh x as follows:

$$\tanh X = \frac{\sinh X}{\cosh X}$$

$$\coth X = \frac{\cosh X}{\sinh X}$$

$$\operatorname{sech} X = \frac{1}{\cosh X}$$

$$\operatorname{csch} X = \frac{1}{\sinh X}$$

The graphs of the hyperbolic functions are shown in Figs. 5-1 through 5-6. The hyperbolic cosine is an even function,  $\cosh(-x) = \cosh x$ , and the hyperbolic sine is an odd function,  $\sinh(-x) = -\sinh x$ . Therefore, one curve is symmetrical about the y-axis and the other is symmetrical with respect to the origin. Here, the hyperbolic functions behave like ordinary trigonometric functions.

The hyperbolic functions are so important that their numerical values have been calculated and tabulated just as have the ordinary trigonometric functions. However, it is very inconvenient to have to stop work and look up a value in a table. Thus, the reason for the following six programs. In this way they can be incorporated directly into a program. As a good example, the impedance of the transmission line in the Gamma and Omega programs was calculated using the hyperbolic cosine.

## Hyperbolic Sine Program

- 5 'HYPERBOLIC SINE
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC SI NE (SINH) OF X"
- 30 INPUT X
- 40 A = ((EXP(1) + X) (EXP(1) + -X))/2
- 50 PRINT"THE HYPERBOLIC SINE OF"X" IS"A

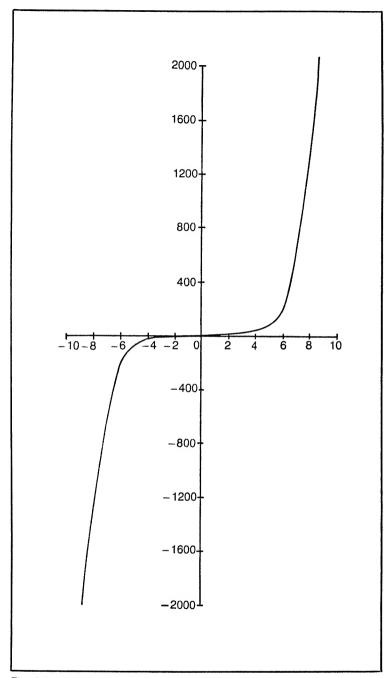


Fig. 5-1. A graph illustrating the hyperbolic sine.

## **Hyperbolic Sine Examples**

ENTER X FOR THE HYPERBOLIC SINE (SINH) OF X ? 9

THE HYPERBOLIC SINE OF 9 IS 4051.54 ENTER X FOR THE HYPERBOLIC SINE (SINH) OF X ? .6

THE HYPERBOLIC SINE OF .6 IS .636654

Note from Fig. 5-1 that with small values of X, the sinh is correspondingly small, greater values of X produce infinitely larger numbers.

# **Hyperbolic Cosine Program**

- 5 'HYPERBOLIC COSINE
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC CO SINE (COSH) OF X"
- 30 INPUT X
- 4Ø A=((EXP(1) ↑ X)+(EXP(1) -X))/2
- 50 PRINT"THE HYPERBOLIC COSINE OF" X"IS"A

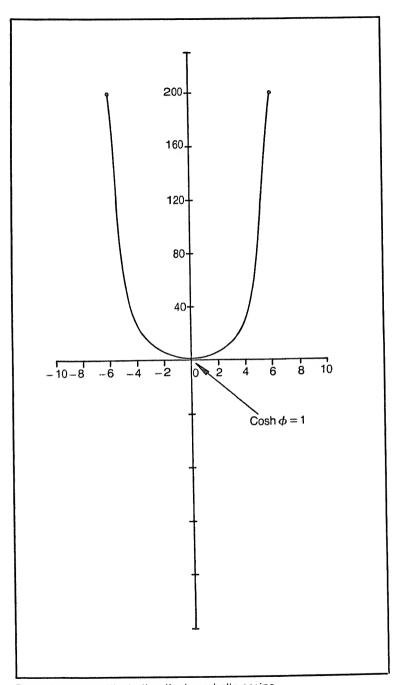


Fig. 5-2. A graph illustrating the hyperbolic cosine.

## **Hyperbolic Cosine Examples**

ENTER X FOR HYPERBOLIC COSINE (COSH) OF X ? -3
THE HYPERBOLIC COSINE OF -3 IS 10.0677
ENTER X FOR HYPERBOLIC COSINE (COSH) OF X ? 0

THE HYPERBOIC COSINE OF 0 IS 1

You'll note that this example shows that the minimum value the hyperbolic cosine can assume is 1. Figure 5-2 also illustrates this fact, showing that the curve is symmetrical about the Y axis.

## **Hyperbolic Tangent Program**

- 5 'HYPERBOLIC TANGENT
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC TA NGENT (TANH) OF X"
- 30 INPUT X
- $A=((EXP(1)^{4}X)-(EXP(1)^{4}-X))/((EXP(1)^{4}X)+(EXP(1)^{4}-X))$
- 50 PRINT"THE HYPERBOLIC TANGENT OF "X"IS"A

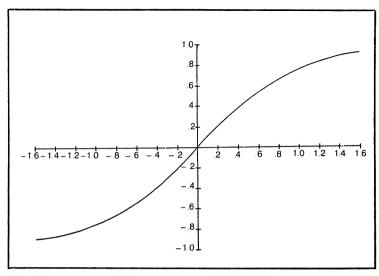


Fig. 5-3. A graph illustrating the hyperbolic tangent.

## **Hyperbolic Tangent Examples**

ENTER X FOR HYPERBOLIC TANGENT (TANH) OF X ? 2

#### THE HYPERBOLIC TANGENT OF 2 IS .964028

As you run a hyperbolic tangent you'll find that it quickly approaches, but never reaches, 1. The TRS-80 is limited in the number of digits it can display. Even using double precision will only allow you to compute a hyperbolic tangent of about 8.3. To use double precision, change lines A in lines 40 and 50 to A#.

## Hyperbolic Cotangent Program

- 5 'HYPERBOLIC COTANGENT
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC CO TANGENT (COTH) OF X"
- 30 INPUT X
- 4D A=((EXP(1)\*X)+(EXP(1)\*--X))/((EXP(1)\*X)-(EXP(1)\*-X))
- 50 PRINT"THE HYPERBOLIC COTANGENT OF X IS A

#### **Hyperbolic Cotangent Examples**

ENTER X FOR HYPERBOLIC COTANGENT (COTH) OF X ? IE-7

THE HYPERBOLIC COTANGENT OF 1E-07 IS 5.59241E+06 ENTER X FOR HYPERBOLIC COTANGENT (COTH) OF X ? 5

#### THE HYPERBOLIC COTANGENT OF 5 IS 1.00009

From these examples and Fig. 5-4 you can see that as the hyperbolic cotangent approaches zero, its value becomes infinitely big, and it approaches 1 as X becomes large.

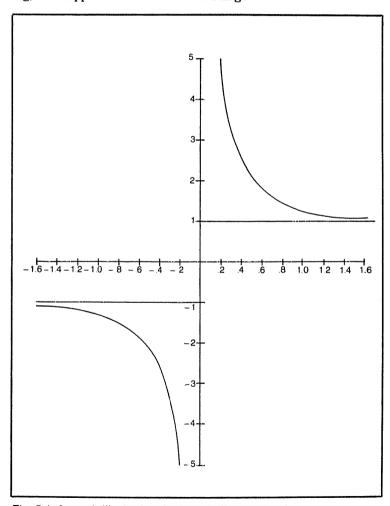


Fig. 5-4. A graph illustrating the hyperbolic cotangent.

## Hyperbolic Secant Program

- 5 'HYPERBOLIC SECANT
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC SE CANT (SECH) OF X"
- 30 INPUT X
- 40 A=2/((EXP(1) + X) + (EXP(1) + -X))
- 50 PRINT"THE HYPERBOLIC SECANT OF" X"IS"A

-

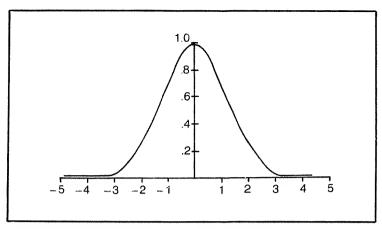


Fig. 5-6. A graph illustrating the hyperbolic secant.

#### **Hyperbolic Secant Examples**

ENTER X FOR HYPERBOLIC SECANT (SECH) OF X ? 0

THE HYPERBOLIC SECANT OF 0 IS 1 ENTER X FOR HYPERBOLIC SECANT (SECH) OF X ? 50

THE HYPERBOLIC SECANT OF 50 IS 3.8575E-22

The maximum value for the hyperbolic secant is one. As X gets increasingly big, either positive or negative, the hyperbolic secant approaches zero.

Generally, the hyperbolic functions behave much like  $e^x/2$ ,  $\bar{e}^x/2$ , unity, or zero as shown in the following table:

$$\begin{array}{lll} X \ (Large \ and \ Positive) & X \ Negative, \ |X| \ Large \\ Cosh \ X \approx sinh x & Cosh \ X \approx -sinh \ X \\ & \approx \frac{1}{2}e^x & \approx \frac{1}{2}e^{-x} \\ tanh \ X \approx coth \ X \approx 1 & tanh \ X \approx coth \approx -1 \\ sech \ X \approx csch \approx & sech \ X \approx -csch \ X \\ & \approx 2e^{-x} \approx 0 & \approx 2e^x \approx 0 \end{array}$$

## Hyperbolic Cosecant Program

- 5 'HYPERBOLIC COSECANT
- 10 CLS
- 20 PRINT"ENTER X FOR HYPERBOLIC CO SECANT (CSCH) OF X"
- 30 INPUT X
- $40 A=2/((EXP(1)^4X)-(EXP(1)^4-X))$
- 50 PRINT"THE HYPERBOLIC COSECANT OF F"X"IS"A

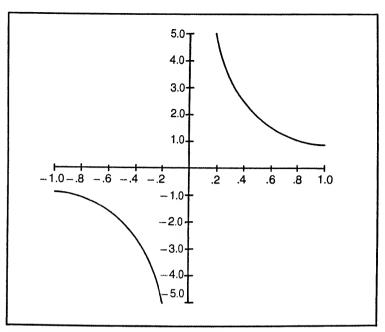


Fig. 5-5. A graph illustrating the hyperbolic cosecant.

#### **Hyperbolic Cosecant Examples**

ENTER X FOR HYPERBOLIC COSECANT (CSCH) OF X ? 2

THE HYPERBOLIC COSECANT OF 2 IS .275721 ENTER X FOR THE HYPERBOLIC COSECANT (CSCH) OF X ? -2

THE HYPERBOLIC COSECANT OF -2 IS -. 275721

The hyperbolic cosecant is very similar to the hyperbolic cotangent, except that instead of being asymptotic to Y=1 it is asymptotic to Y=0. Again, as the value of X gets smaller, the hyperbolic cosecant becomes infinitely big.

#### INVERSE HYPERBOLIC FUNCTIONS

The inverse hyperbolic functions perform the inverse operation of the hyperbolic functions. That is, if you compute  $X = \sinh Y$ , then the inverse hyperbolic secant is  $Y = \sinh^{-1} X$ . The general curves for the inverse hyperbolic functions are shown in Fig. 5-7 through 5-12.

To compute the inverse hyperbolic functions, use the following formulas:

$$sinh^{-1} x = ln (x + (x^{2} + 1)^{-5})$$

$$tanh^{-1} x = \frac{1}{2} (n (\frac{1+x}{1-x}))$$

$$sech^{-1} x = ln (\frac{1}{x} + (\frac{1}{x^{2}} - 1)^{-5})$$

$$cosh^{-1} x^{2} = sech^{-1} \frac{1}{x}$$

$$coth^{-1} x^{2} = tcnh^{-1} \frac{1}{x}$$

$$csch^{-1} x^{2} = sinh^{-1} \frac{1}{x}$$

## **Inverse Hyperbolic Sine Program**

- 5 'INV. HYPERBOLIC SINE
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC SINE OF X"
- 3Ø INPUT X
- 40 A=LOG(X+((X42)+1)4.5)
- 5Ø PRINT"THE INVERSE HYPERBOLIC SI NE OF"X"IS"A

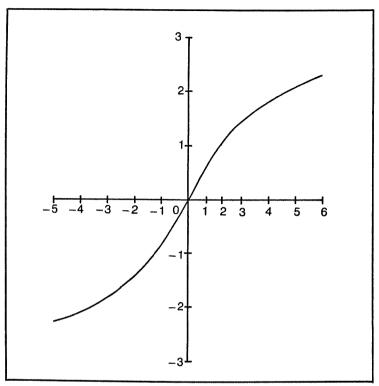


Fig. 5-7. A graph illustrating the inverse hyperbolic sine.

# **Inverse Hyperbolic Sine Examples**

ENTER X FOR INVERSE HYPERBOLIC SINE OF X ? 5

THE INVERSE HYPERBOLIC SINE OF 5 IS 2.3124 ENTER X FOR INVERSE HYPERBOLIC SINE OF X ? -5

THE INVERSE HYPERBOLIC SINE OF -5 IS -2.3124

These examples show that the inverse hyperbolic sine is a single value; that is, as X varies, Y produces a different answer for each value of X. The curve does not reverse to produce the same value for X as for -X.

## Inverse Hyperbolic Cosine Program

- 5 'INV. HYPERBOLIC COSINE
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC COSINE OF X"
- 30 INPUT X
- 40 A=LOG(X+((XE2)-1)4.5)
- 50 PRINT"THE INVERSE HYPERBOLIC CO SINE OF "X" IS" A 45B = - A

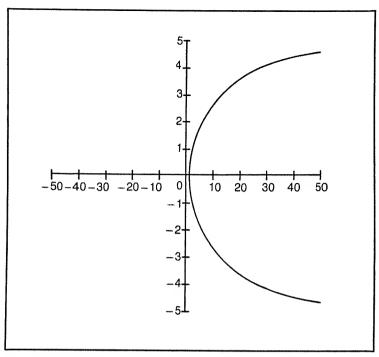


Fig. 5-8. A graph illustrating the inverse hyperbolic cosine.

## **Inverse Hyperbolic Cosine Examples**

ENTER X FOR INVERSE HYPERBOLIC COSINE OF X ? . 5

?FC ERROR IN 40

Whereas  $\cosh \emptyset = 1$ , the inverse hyperbolic function is limited to the range of greater than one.

ENTER X FOR INVERSE HYPERBOLIC COSINE OF X ? 20

THE INVERSE HYPERBOLIC COSINE OF 20 IS 3.68825 AND -3.68825

Note that in the solution for the inverse hyperbolic cosine, for each value of X there are two corresponding values for Y.

## Inverse Hyperbolic Tangent Program

- 5 'INV. HYPERBOLIC TANGENT
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC TANGENT OF X"
- 30 INPUT X
- 40 A=.5\*LOG((1+X)/(1-X))
- 50 PRINT"THE INVERSE HYPERBOLIC TA NGENT OF "X" IS "A

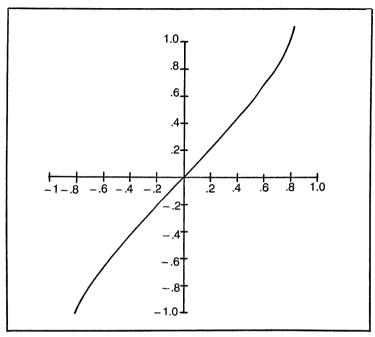


Fig. 5-9. A graph illustrating the inverse hyperbolic tangent.

## **Inverse Hyperbolic Tangent Examples**

ENTER X FOR INVERSE HYPERBOLIC TANGENT OF X ?.4

THE INVERSE HYPERBOLIC TANGENT OF .4 IS .423649 ENTER X FOR INVERSE HYPERBOLIC TANGENT OF X ? .1

THE INVERSE HYPERBOLIC TANGENT OF .1 IS .100335

You'll note from these two examples and the curve shown in Fig. 5-9 that the inverse hyperbolic tangent is *almost* a straight-line function. However, as X approaches 1, the function becomes asymptotic to at the X=1 and X=-1 lines.

## Inverse Hyperbolic Cotangent Program

- 5 'INV. HYPERBOLIC COTANGENT
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC COTANGENT OF X"
- 30 INPUT X
- 40 A=.5\*LOG((1+1/X)/(1-1/X))
- 50 PRINT"THE INVERSE HYPERBOLIC CO TANGENT OF "X" IS "A

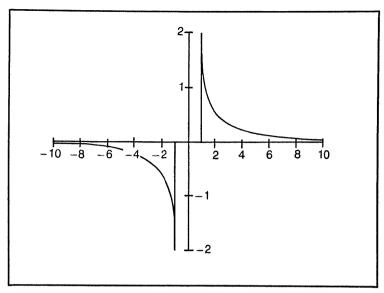


Fig. 5-10. A graph illustrating the inverse hyperbolic cotangent.

## **Inverse Hyperbolic Cotangent Examples**

ENTER X FOR INVERSE HYPERBOLIC COTANGENT OF X ? .5

?FC ERROR IN 40

This shows that the function  $Y = \coth^{-1} X$  is only valid for X greater than 1 and X less than -1. The region running from -1 through 0 to 1 is invalid.

ENTER X FOR INVERSE HYPERBOLIC COTANGENT OF X ? -6

THE INVERSE HYPERBOLIC COTANGENT OF -6 IS -.168236

## Inverse Hyperbolic Secant Program

- 5 'INV. HYPERBOLIC SECANT
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC SECANT OF X"
- 30 INPUT X
- 4Ø A=LOG(1/X+(((1/X↑2))-1)4.5)
- 45 B=-A
- 50 PRINT"THE INVERSE HYPERBOLIC SE CANT OF "X" IS "A" AND " B

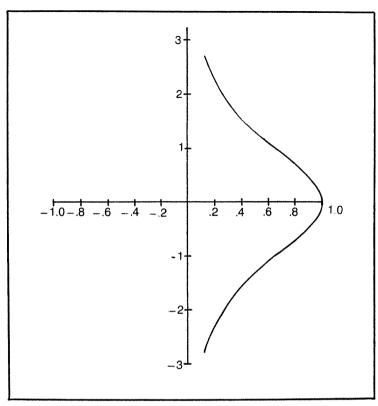


Fig. 5-11. A graph illustrating the inverse hyperbolic secant.

## **Inverse Hyperbolic Secant Examples**

ENTER X FOR INVERSE HYPERBOLIC SECANT OF X ? 1

THE INVERSE HYPERBOLIC SECANT OF 1 IS Ø ENTER X FOR INVERSE HYPERBOLIC SECANT OF X ?.6

THE INVERSE HYPERBOLIC SECANT OF .6 IS 1.09861 AND -1.09861

The inverse hyperbolic secant acts in the same manner as the inverse hyperbolic cosine. Each unique value of X produces two answers, Y and -Y. Small values of X eventually become asymptotic to the Y axis, both plus and minus (see Fig. 5-11).

## Inverse Hyperbolic Cosecant Program

- 5 'INV. HYPERBOLIC COSECANT
- 10 CLS
- 20 PRINT"ENTER X FOR INVERSE HYPER BOLIC COSECANT OF X"
- 30 INPUT X
- 4Ø A=LOG(1/X+(((1/X+2))+1)4.5)
- 50 PRINT"THE INVERSE HYPERBOLIC CO SECANT OF "X" IS" A

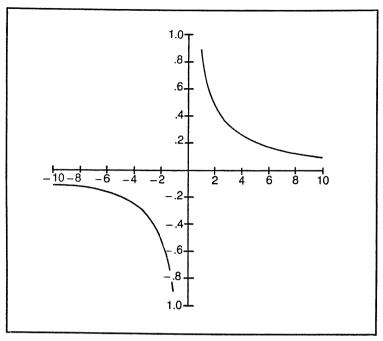


Fig. 5-12. A graph illustrating the inverse hyperbolic cosecant.

## **Inverse Hyperbolic Cosecant Examples**

ENTER X FOR INVERSE HYPERBOLIC COSECANT OF X ? 0

?/Ø ERRORIN40

ENTER X FOR INVERSE HYPERBOLIC COSECANT OF X ? 8

# THE INVERSE HYPERBOLIC COSECANT OF 8 IS . 124677

The curve of the inverse hyperbolic cosecant is not unlike the curve of the inverse hyperbolic cotangent. However, instead of small values of X becoming asymptotic to X=1, the curve is asymptotic to the Y axis. Large values of X eventually become asymptotic to the X axis (see Fig. 5-12).

#### **COMPLEX FUNCTIONS**

where

where

 $sgn(Y) = 1 if y \ge 0$ -1 if v = 0

The next twelve programs deal with the complex trigonometricfunctions, or the sine, cosine, ... of complex numbers and the inverse trigonometric functions.

The equations to solve each of the following programs are:

$$\sin(x + iy) = \sin x \cosh Y + i \cos x \sinh Y$$

$$\cos(x + iY) = \cos x \cosh Y - i \sin x \sinh Y$$

$$\tan(x + iy) = \frac{\sin 2x + i \sinh 2Y}{\cos 2x + \cosh 2Y}$$

$$\cot(x + iy) = \frac{\sin 2x - i \sinh 2Y}{\cosh 2x - \cos 2Y}$$

$$\csc(x + iy) = \frac{1}{\sin(x + iY)}$$

$$\sec(x + iy) = \frac{1}{\cos(x + iY)}$$

$$\sin^{-1}(x + iy) = \sin^{-1}B + i \operatorname{sgn}(y) \operatorname{1n}(A + \sqrt{A^2 - 1})$$
here
$$A = \frac{1}{2}\sqrt{(X + 1)^2 + y^2} + \frac{1}{2}\sqrt{(c - 1)^2 + y^2}$$

$$\operatorname{sgn}(Y) = \operatorname{1if} y \geqslant 0$$

$$-\operatorname{1if} y = 0$$

$$-\operatorname{1if} y = 0$$

$$\cos^{-1}(x + iy) = \cos^{-1}B + i \operatorname{sgn}(d) \operatorname{1n}(A + \sqrt{A^2 - 1})$$
here
$$A = \frac{1}{2}\sqrt{(x + 1)^2 + y^2} + \frac{1}{2}\sqrt{(c - 1)^2 + y^2}$$

 $B = \frac{1}{2} \sqrt{(x+1)^2 + v^2} - \frac{1}{2} \sqrt{(c-1)^2 + v^2}$ 

$$\tan^{-1}(x + iy) = \frac{1}{2} \left( \pi - \tan^{-1} \frac{1+y}{A} - \tan^{-1} \frac{1-B}{A} + \frac{t}{4} \right)$$

$$\ln \left( \frac{(1+y)^2 + x^2}{(1-y)^2 + x^2} \right)$$

$$\cot^{-1}(x + iy) = \frac{\pi}{2} - \tan^{-1}(x + iy)$$

$$\csc^{-1}(x+iy) = \sin^{-1}\left(\frac{1}{x+iy}\right)$$

$$\sec^{-1}(x+iy) = \cos^{-1}\left(\frac{1}{x+iy}\right)$$

#### **Complex Sine Program**

- 5 'COMPLEX SINE
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUNBER (REA L, IMAGINARY)"
- 30 INPUT R, I
- 4Ø AR=SIN(R)\*((EXP(1) I+EXP(1) I-I)
  /2)
- 5Ø AI=COS(R)\*((EXP(1) ↑ I-EXP(1) ↑ -I)
  /2)
- 60 PRINT"THE COMPLEX SINE IS"AR; AI

### **Complex SineExamples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 2, -3
THE COMPLEX SINE IS 9.1545 4.16891
ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 3, -4
THE COMPLEX SINE IS 3.85374 27.0168

#### **Complex Cosine Program**

- 5 'COMPLEX COSINE
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)"
- 30 INPUT R, I
- 4Ø AR=COS(R)\*((EXP(1) ↑ I+EXP(1) ↑ -I)
  /2)
- 50 AI=-(SIN(R)\*((EXP(1)\*I-EXP(1)\*-I)/2))
- 60 PRINT"THE COMPLEX COSINE IS"AR; AI"I"

## **Complex Cosine Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 2, -3
THE COMPLEX COSINE IS 4.18963 9.10923
ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? -.2, 5
THE COMPLEX COSINE IS 72.7307 14.7419

#### **Complex Tangent Program**

- 5 'COMPLEX TANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REA L, IMAGINARY)"
- 30 INPUT R.I
- 4Ø D=COS(2\*R)+((EXP(1) (2\*I)+EXP(1 1 (2\*-I))/2)
- 50 AR=SIN(2\*R)/(D)
- 40 AI=((EXP(1) ↑ (2\*I) + EXP(1) ↑ (2\*-I) )/2)/(D)
- 70 PRINT"THE COMPLEX TANGENT IS"AR ;AI"i"

### **Complex Tangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ?-2,-3THE COMPLEX TANGENT IS 3.76403E-03 1.00325

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?10, -5

THE COMPLEX TANGENT IS 8.28923E-05.999963

## **Complex Cotangent Program**

- 5 'COMPLEX COTANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUNBER (REA L, IMAGINARY)"
- 30 INPUT RI
- 4Ø D=-COS(2\*R)+((EXP(1)\*(2\*I)+EXP( 1/\*(2\*-I))/2)
- 50 AR=SIN(2\*R)/(D)
- 60 AI=-((EXP(1) ↑ (2\*I)-EXP(1) ↑ (2\*-I))/2)/(D)
- 70 PRINT"THE COMPLEX COTANGENT IS" AR; AI" i"

### **Complex Cotangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)
? 2,3
THE COMPLEX COTANGENT IS 3.73971E-03 -.996758
ENTER COMPLEX NUMBER (REAL, IMAGINARY)
? - 12, .3
THE COMPLEX CONTANGENT IS 1.18954 - .836285

### **Complex Secant Program**

- 5 'COMPLEX SECANT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUNBER (REAL, IMAGINARY)"
- 30 INPUT R, I
- 4Ø AR=COS(R)\*((EXP(1) ↑ I+EXP(1) ↑ -I)
  /2)
- 50 AI=-(SIN(R)\*((EXP(1) ↑ I-EXP(1) ↑ I)/2))
- 60 M=SQR(AR[2+AI+2)
- 70 T=ATN(AI/AR)
- 80 FR=1/M\*(COS(-T))
- 90 FI=1/M\*(SIN(-T))
- 100 PRINT"THE COMPLEX SECANT IS"FR ;FI

## **Complex Secant Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)
? 4, -9
THE COMPLEX SECANT IS 1.61332E-04 -1.86794E-04
ENTER COMPLEX NUMBER (REAL, IMAGINARY)
? -.009, 10
THE COMPLEX SECANT IS 9.07961E-05 -8.17201E-07

# **Complex Cosecant Program**

- 5 'COMPLEX COSECANT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)"
- 30 INPUT R, I
- 4Ø AR=SIN(R)\*((EXP(1) | I+EXP(1) | -I)
  /2)
- 50 AI=COS(R)\*((EXP(1) $\uparrow$  I-EXP(1) $\uparrow$ -I)
  /2)
- 60 M=S@R(AR[2+A] ↑2)
- 70 T=ATN(AI/AR) -
- 80 FR=1/M\*(COS(-T))
- 90 FI=1/M\*(SIN(-T))
- 100 PRINT"THE COMPLEX COSECANT IS" FR:FI

### **Complex Cosecant Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)
? 3, -.5
THE COMPLEX COSECANT IS .545987 - 1.77002
? -.3, 10
THE COMPLEX COSECANT IS 2.68332E-05 8.67444E-05

#### **Complex Arc Sine Program**

```
5 'COMPLEX ARC SINE
10 CLS
20 PRINT"ENTER COMPLEX NUMBER (REA
    L, IMAGINARY)
30 INPUT R.I
4Ø M=SQR((R+1) ∮2+(I∮2))
50 \text{ N=SQR}((R-1) \land 2+(I \land 2))
60 \ Z(1) = .5 * M + .5 * N
70 \text{ Z}(2) = .5 \times -M + .5 \times N
80 \ Z(3) = .5 \times M + .5 \times -N
90 \ Z(4) = .5 \times -M + .5 \times -N
100 \ Z(5) = .5 \times M - .5 \times N
110 \ Z(6) = .5 \times -M - .5 \times N
120 Z(7) = .5 \times M - .5 \times -N
130 \ Z(8) = .5 \times -M - .5 \times -N
140 FOR P=5 TO 8
145 IF Z(P)<0 GOTO 160
146 IF Z(P)>1 GOTO 160
150 AR(P) = ATN(Z(P)/SQR(-Z(P)*Z(P)+
     1))
160 NEXT P
170 IF I=>0 THEN S=1 :STOPS=-1
180 FOR P=1 TO 4
185 IF Z(P) (1 GOTO 210)
190 A1(P)=(LOG(Z(P)+SQR(Z(P)\neq 2-1))
     ) *S
200 \text{ A2(P)} = (\text{LOG(Z(P)} - \text{SQR(Z(P)} + 2-1)))
     ) *S
210 NEXT P
220 PRINT"THE COMPLEX ARC SINE IS
     ..... #
230 FOR P=5 TO 8
240 IF AR(P)=0 GOTO300
25Ø FOR G=1 TO 4
260 IF A1(G)=0 G0T0290
270 PRINTAR(P), A1(G)
280 PRINTAR(P), A2(G)
290 NEXT G
300 NEXT P
```

### **Complex Arc Sine Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

? 5, 8

THE COMPLEX ARC SINE IS -

.556083 2.93872

.556083 - 2.93872

Note that all the inverse complex trigonometric functions are double-valued.

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?1.-2

THE COMPLEX ARC SINE IS -

.4247079 - 1.52857

.427079 1.52857

#### **Complex Arc Cosine Program**

```
5 'COMPLEX ARC COSINE
10 CLS
20 PRINT"ENTER COMPLEX NUMBER (REA
    L, IMAGINARY)
30 INPUT R, I
4Ø M=SQR((R+1) 4 2+(T42))
50 \text{ N=SQR}((R-1) \triangleq 2 + (I \triangleq 2))
607.7(1) = .5 \times M + .5 \times N
70 \ Z(2) = .5 \times -M + .5 \times N
80 \ Z(3) = .5 \times M + .5 \times -N
90 \ Z(4) = .5 \times -M + .5 \times -N
100 \ Z(5) = .5 \times M - .5 \times N
110 \ Z(6) = .5 \times -M - .5 \times N
120 Z(7) = .5 \times M - .5 \times -N
130 \ Z(8) = .5 \times -M - .5 \times -N
14Ø FOR P=5 TO 8
145 IF Z(P)<0 GOTO 160
146 IF Z(P)>1 GOTO 160
150 AR(P) = -ATN(Z(P)/SQR(-Z(P)*Z(P))
     +1))+1.5708
160 NEXT P
170 IF I=>0 THEN S=1 ELSE S=-1
180 FOR P=1 TO 4
185 IF Z(P)<1 GOTO 210
190 A1(P)=-(LOG(Z(P)+SQR(Z(P)\neq2-1)
     ))*S
200 \text{ A2(P)} = -(\text{L0G(Z(P)} - \text{SQR(Z(P)} / 2-1))
     ))*S
210 NEXT P
220 PRINT"THE COMPLEX ARC COSINE I
     S --"
230 FOR P=5 TO 8
240 IF AR(P)=0 GOTO300
250 FOR G=1 TO 4
260 IF A1(G)=0 G0T0290
270 PRINTAR(P), A1(G)
280 PRINTAR(P), A2(G)
290 NEXT G
300 NEXT P
```

### **Complex Arc Cosine Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?1, -2

THE COMPLEX ARC COSINE IS -

1.14372 1.52857

1.14872 - 1.52857

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

? 23,8

THE COMPLEX ARC COSINE IS -

.334995 -3.88541

.334995 3.88556

## **Complex Arc Tangent Program**

- 5 'COMPLEX ARC COTANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REA L, IMAGINARY)
- 30 INPUT R, I
- 40 AR=.5\*(3.14159-ATN((1+I)/R)-ATN ((1-I)/R))
- 50 AI=LOG((((1+I)[2+R[2)/((1-I)|2+R |42))/4
- 60 PRINT"THE COMPLEX ARC COTANGENT IS --"
- 70 PRINT3.14159/2-AR, AI

# **Complex Arc Tangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 5, 8 THE COMPLEX ARC TANGENT IS — 1.51422 .0898434 1.51422 -.0898434

# **Complex Arc Cotangent Program**

- 5 'COMPLEX ARC COTANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)
- 30 INPUT R, I
- 4Ø AR=.5\*(3.14159-ATN((1+I)/R)-ATN ((1-I)/R))
- 50 AI=LOG((((1+I)[2+R[2)/((1-I) ↑2+R ↑2))/4
- 60 PRINT"THE COMPLEX ARC COTANGENT IS --"
- 70 PRINT3.14159/2-AR, AI

# **Complex Arc Cotangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?2,3

THE COMPLEX ARC COTANGENT IS -

.160875 -.229073

.160875 .229073

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?1,1

THE COMPLEX ARC COTANGENT IS -

.553574 .40236

.553574 -.40236

#### **Complex Arc Secant Program**

```
5 'COMPLEX ARC SECANT
10 CLS
20 PRINT"ENTER COMPLEX NUMBER (REAL)
    IMAGINARY)
30 INPUT R.I
35 GOSUB 310
40 M=SQR((R+1)[2+(I[2))
50 \text{ N=SQR}((R-1)[2+(T[2))]
60.7(1) = .5 \times M + .5 \times N
70 \text{ Z}(2) = .5 \times -M + .5 \times N
80 \ Z(3) = .5 \times M + .5 \times -N
90.7(4) = .5 \times -M + .5 \times -N
100 \ Z(5) = .5 \times M - .5 \times N
110 Z(6) = .5 \times -M - .5 \times N
120 Z(7) = .5 * M - .5 * - N
130 \ Z(8) = .5 \times -M - .5 \times -N
140 FOR P=5 TO 8
145 IF Z(P)<0 GOTO 160
146 IF Z(P)>1 GOTO 160
150 AR(P) = -ATN(Z(P)/SQR(-Z(P)*Z)
     (P)+1))+1.5708
160 NEXT P
170 IF I=>0 THEN S=1 ELSE S=-1
180 FOR P=1 TO 4
185 IF Z(P)<1 GOTO 210
190 A1(P)=-(LOG(Z(P)+SQR(Z(P)^{\dagger}2-1)))*S
200 \text{ A2(P)} = -(\text{LOG(Z(P)} - \text{SQR(Z(P)} + 2-1))) *S
210 NEXT P
220 PRINT"THE COMPLEX ARC SECANT IS --
230 FOR P=5 TO 8
240 IF AR(P)=0 GOTO300
25Ø FOR G=1 TO 4
260 IF A1(G)=0 G0T0290
270 PRINTAR(P), A1(G)
280 PRINTAR(P), A2(G)
290 NEXT G
300 NEXT P
305 END
310 F=SQR(RD2+ID2)
```

320 T=ATN(I/R)

330 F=1/F

340 T=-T

350 R=F\*COS(T)

360 I=F\*SIN(T)

370 RETURN

# **Complex Arc Secant Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?8,-5

THE COMPLEX ARC SECANTIS —

1.48093 -.0563788

1.48093 .0563784

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

? - .03, .03

THE COMPLEX ARC SECANTIS --

.785853 - 3.85313

.785853 3.85321

#### **Complex Arc Cosecant**

```
5 'COMPLEX ARC COSECANT
10 CLS
20 PRINT"ENTER COMPLEX NUMBER (REA
   L, IMAGINARY)
30 INPUT R.I
35 GOSUB 310
4D M = SOR((R+1) \neq 2 + (I \neq 2))
50 N=SQR((R-1) \nmid 2+(I \nmid 2))
60 \ Z(1) = .5 * M + .5 * N
70/7(2) = .5 \times -M + .5 \times N
80 Z(3) = .5*M + .5* - N
90 \ Z(4) = .5 \times -M + .5 \times -N
100 \ Z(5) = .5 * M - .5 * N
110 \ Z(6) = .5 \times -M - .5 \times N
120 Z(7) = .5 \times M - .5 \times -N
130 Z(8) = .5 * - M - .5 * - N
140 FOR P=5 TO 8
145 TE Z(P)<0 GOTO 160
146 IF Z(P)>1 GOTO 160
150 AR(P) = ATN(Z(P)/SQR(-Z(P)*Z(P)*
     1))
140 NEXT P
170 IF I=>0 THEN S=1 ELSE S=-1
180 FOR P=1 TO 4
185 IF Z(P)<1 GOTO 210
190 A1(P)=(LOG(Z(P)+SQR(Z(P)*2-1))
200 \text{ A2(P)} = (\text{LOG}(\text{Z(P)} - \text{SQR}(\text{Z(P)} \bullet 2 - 1))
     ) *S
210 NEXT P
220 PRINT"THE COMPLEX ARC COSECANT
       TS --"
230 FOR P=5 TO 8
240 IF AR(P)=0 G0T0300
250 FOR G=1 TO 4
260 IF A1(G)=0 G0T0290
270 PRINTAR(P) + A1(G)
280 PRINTAR(P), A2(G)
290 NEXT G
300 NEXT P
```

- 305 END
- 310 F=S0R(RE2+IE2)
- 320 T=ATN(I/R)
- 330 F=1/F
- 340 T=-T
- 350 R=F\*COS(T)
- 360 I=F\*SIN(T)
- 370 RETURN

## **Complex Arc Cosecant Examples**

? 5, 8

THE COMPLEX ARC COSECANT IS -

.0559826 -.089909

.0559826 .0899086

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?-2,3

THE COMPLEX ARC COSECANT IS —

.150386 .231335

.150386 -.231335

#### **COMPLEX HYPERBOLIC FUNCTIONS**

The last group of trigonometric function programs are the complex hyperbolic functions. Programs to solve the complex hyperbolic functions are:

```
\sinh(x+iY) = -i \sin i (x+iY)
\cosh(x+iY) = \cos i (x+iy)
\tanh(x+iY) = -i \tan i (x+iY)
\coth(x+iY) = i \cot i (x+iY)
\operatorname{csch}(x+iy) = i \csc i (x+iY)
\operatorname{sech}(x+iy) = \operatorname{sec} i (x+iY)
```

### **Complex Hyperbolic Sine Program**

- 5 'COMPLEX HYPERBOLIC SINE
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)"
- 30 INPUT I:R
- 4Ø AR=SIN(R)\*((EXP(1) | I+EXP(1) | -I) /2)
- 5Ø AI=COS(R)\*((EXP(1)\*I-EXP(1)\*-I)
  /2)
- 60 PRINT"THE COMPLEX HYPERBOLIC SI NE IS"AI; AR"I"

### **Complex Hyperbolic Sine Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?3,3

THE COMPLEX HYPERBOLIC SINE IS -9.91762 1.42075 ENTER COMPLEX NUMBER (REAL, IMAGINARY)

? - 3, -3

THE COMPLEX HYPERBOLIC SINE IS 9.91762 -1.42075

# **Complex Hyperbolic Cosine Program**

- 5 'COMPLEX HYPERBOLIC COSINE
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUMBER (REA L, IMAGINARY)"
- 30 INPUT I,R
- 40 AR=COS(R)\*((EXP(1) I+EXP(1) -1)
  /2)
- 5Ø AI=(SIN(R)\*((EXP(1) I -EXP(1) I -I )/2))
- 60 PRINT"THE COMPLEX HYPERBOLIC CO SINE IS"AR;AI"!"

#### Complex Hyperbolic Cosine Examples

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

0 3, 2

THE COMPLEX HYPERBOLIC COSINE IS -4.18963 9.10923 ENTER COMPLEX NUMBER (REAL, IMAGINARY)

0 2, 3

THE COMPLEX HYPERBOLIC COSINE IS -3.72455 .511823

### **Complex Hyperbolic Tangent Programs**

- 5 'COMPLEX HYPERBOLIC TANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUNBER (REAL, IMAGINARY)"
- 3Ø INPUT I,R
- 4Ø D=COS(2\*R)+((EXP(1))♠(2\*I)+EXP(1))♠(2\*-I))/2)
- 50 AR=SIN(2\*R)/(D)
- 6Ø AI=((EXP(1) (2\*I)+EXP(1) (2\*-I) )/2)/(D)
- 7Ø PRINT"THE COMPLEX HYPERBOLIC TA NGENT IS"AI;AR"!"

## **Complex Hyperbolic Tangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

? 1,2

THE COMPLEX HYPERBOLIC TANGENT IS 1.21027 -.243458

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 5,-3

THE COMPLEX HYPERBOLIC TANGENT IS .999913 2.53687E-05

#### **Complex Hyperbolic Cotangent Program**

- 5 'COMPLEX HYPERBOLIC COTANGENT
- 10 CLS
- 20 PRINT"ENTER COMPLEX NUNBER (REAL, IMAGINARY)"
- 30 INPUT I,R
- 4Ø D=COS(2\*R)-((EXP(1)\*(2\*I)+EXP(1)\*(2\*-I))/2)
- 50 AR=SIN(2\*R)/(D)
- 6Ø AI=-((EXP(1))(2\*I)-EXP(1))(2\*-I))/2)/(D)
- 70 PRINT"THE COMPLEX HYPERBOLIC CO TANGENT IS"AI;AR"i"

# **Complex Hyperbolic Cotangent Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 3,4

THE COMPLEX HYPERBOLIC COTANGENT IS .999267 -4.90118E-03

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 1,10

THE COMPLEX HYPERBOLIC COTANGENT IS 1.08132 -.272187

#### Complex Hyperbolic Secant Program

5 'COMPLEX HYPERBOLIC SECANT
10 CLS
20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)"
30 INPUT I,R
40 AR=COS(R)\*((EXP(1)\*I+EXP(1)\*-I)/2)
50 AI=-(SIN(R)\*((EXP(1)\*I-EXP(1)\*-I)/2))
60 M=SQR(AR\*2+AI\*2)
70 T=ATN(AI/AR)
80 FR=-1/M\*(COS(-T))
90 FI=1/M\*(SIN(-T))
100 PRINT"THE COMPLEX HYPERBOLIC SECANT IS"FR;FI

#### **Complex Hyperbolic Secant Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 1. 2

THE COMPLEX HYPERBOLIC SECANT IS -.413149 -.687527 ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 2.1

THE COMPLEX HYPERBOLIC SECANT IS -. 151176 .226974

This completes the programs and examples for the trigonometric functions. Though each is short, the basic equations and examples have been given to aid in understanding. Additionally, the computational part of the programs can be incorporated into larger, more complex programs.

## **Complex Hyperbolic Cosecant Program**

5 'COMPLEX HYPERBOLIC COSECANT

10 CLS

20 PRINT"ENTER COMPLEX NUMBER (REAL, IMAGINARY)"

30 INPUT I,R

40 AR=SIN(R)\*((EXP(1)\*I+EXP(1)\*-I)/2)

50 AI=COS(R)\*((EXP(1)\*I-EXP(1)\*-I)/2)

60 M=SQR(AR\*2+AI\*2)

70 T=ATN(AI/AR)

80 FR=-1/M\*(COS(-T))

90 FI=-1/M\*(SIN(-T))

100 PRINT"THE COMPLEX HYPERBOLIC COSECANT IS"FI;FR

## **Complex Hyperbolic Cosecant Examples**

ENTER COMPLEX NUMBER (REAL, IMAGINARY)

?4.5

THE COMPLEX HYPERBOLIC COSECANT IS -.0103816 -.0351186

ENTER COMPLEX NUMBER (REAL, IMAGINARY) ? 5, 4

THE COMPLEX HYPERBOLIC COSECANT IS 8.80791E-03 -.0101989

## **TRIANGLES**

The next four programs in this chapter deal with solving triangle problems. They are especially useful in surveying work. Solving for the unknown sides and angles of oblique triangles depends upon using the Law of Sines and Law of Cosines which are:

Law of Sines 
$$-\frac{1}{\sin A} = \frac{b}{\sin B} = \frac{c}{\sin C}$$

Law of Cosines -  $c^2 = a^2 + b^2 - 2ab \cos C$ 

## Two Sides, Non-Included Angle Program

- 5 '2 SIDES, NON-INCLUDED ANGLE
- 10 CLS
- 20 PRINT"ENTER THE TWO SIDES AND THE NON-INCLUDED ANGLE"
- 25 PRINT"ENTER FIRST SIDE, SECOND SIDE AND ITS ASSOCIATED ANGLE"
- 30 INPUT BS, AS, AA
- 31 QA=AA
- 35 AA=AA\*. Ø1745329
- 4Ø Z=BS\*SIN(AA)/AS
- 5Ø BA=ATN(Z/SQR(-Z\*Z+1))\*57.29578
- 60 CA=180-QA-BA
- 65 CA=CA\*.01745329
- 7Ø CS=AS\*SIN(CA)/SIN(AA)
- 90 PRINT"THE THIRD SIDE IS"CS", IT S ASSOCIATED ANGLE IS"CA\*57.295 78CHR\$(13)"DEGREES AND THE FIRS T SIDE'S ASSOCIATED ANGLE IS"BA CHR\$(13)"DEGREES."
- 100 IF QA<90 AND AS<BS GOTO 110 EL SE END
- 110 PRINT"A SECOND SOLUTION EXISTS FOR THIS TRIANGLE."
- 120 BA=180-BA
- 130 CA=180-BA-AA\*57.29578
- 140 CS=AS\*SIN(CA\*.01745329)/SIN(AA)

150 PRINT"FOR THE SECOND SOLUTION,
THE THIRD SIDE IS"CS", ITS"CH
R\$(13)"ASSOCIATED ANGLE IS"CA"
DEGREES AND THE FIRST SIDE'S"C
HR\$(13)"ASSOCIATED ANGLE IS"BA

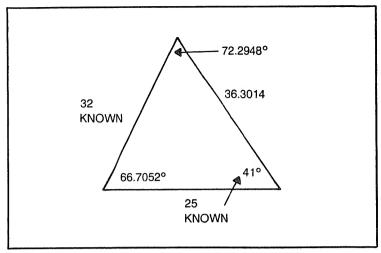


Fig. 5-13. A triangle with two known sides and a non-included angle.

## Two Sides, Non-Included Angle Example

Using Fig. 5-13, solve for the unknown sides and angles. ENTER THE TWO SIDES AND THE NON-INCLUDED ANGLE ENTER FIRST SIDE, SECOND SIDE AND ITS ASSOCIATED ANGLE

? 35,25,41

THE THIRD SIDE IS 36.3014, ITS ASSOCIATED ANGLE IS 72.2948

DEGREES AND THE FIRST SIDE'S ASSOCIATED ANGLE IS 66.7052

DEGREES.

A SECOND SOLUTION EXISTS FOR THIS TRIANGLE.

FOR THE SECOND SOLUTION, THE THIRD SIDE IS 16.5283, ITS ASSOCIATED ANGLE IS 25.7052 DEGREES AND THE FIRST SIDE'S

ASSOCIATED ANGLE IS 113.295

This example illustrates that it is possible to have two solutions for this triangle. When using degrees, they must be in a decimal format, not minutes and seconds.

## **Three Sides Program**

- 5 '3 SIDES
- 10 CLS
- 20 INPUT"ENTER THE THREE SIDES OF THE TRIANGLE"; A, B, C
- $30 D = (A \cdot 2 + B \cdot 2 C \cdot 2) / (2 * A * B)$
- 40 CA=-ATN(D/SQR(-D\*D+1))+1.5708
- 50 Z=SIN(CA)/C
- 60 CA=CA\*57.29578
- 70 BA=ATN((B\*Z)/SQR(-B42\*Z\*Z+1))
- 80 BA=BA\*57.29578
- 90 AA=ATN((A\*Z)/SQR(-A +2\*Z\*Z+1))
- 100 AA=AA\*57.29578
- 110 PRINT"THE THREE CORRESPONDING ANGLES (A,B,C) ARE"CHR\$(13)AA" DEGREES"CHR\$(13)BA"DEGREES"CHR \$(13)CA"DEGREES"

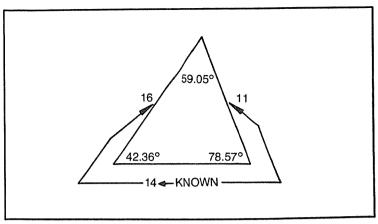


Fig. 5-14. A triangle with three sides, unknown angles.

## **Three Sides Example**

In this example, the three sides are known, and you must determine the three included angles (use Fig. 5-14). ENTER THE THREE SIDES OF THE TRIANGLE?

? 11, 14, 16

THE THREE CORRESPONDING ANGLES (A, B, C) ARE

**42.3674 DEGREES** 

59.0558 DEGREES

78.5771 DEGREES

## Two Angles and Opposite Side Program

- 5 '2 SIDES, OPPOSITE ANGLE
- 10 CLS
- 20 INPUT"ENTER THE TWO ANGLES (A,B) AND THE OPPOSITE SIDE"; AA,BA,CS
- 30 CA=180-AA-BA

- 40 BS=CS\*SIN(BA/57.29578)/SIN(AA/5 7.29578)
- 50 CS=CS\*SIN(CA/57.29578)/SIN(AA/5 7.29578)
- 60 PRINT"THE THIRD ANGLE IS"CA"DEG REES AND THE TWO UNKNOWN OPPOSI TE"CHR\$(13)"SIDES ARE"BS"AND"CS

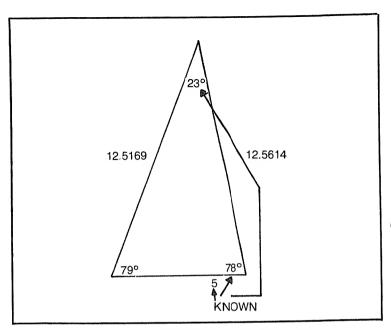


Fig. 5-15. A triangle with two known sides, opposite angles.

## Two Angles and Opposite Side Example

Using Fig. 5-15, solve for the remaining angle and two sides. ENTER THE TWO ANGLES (A,B) AND THE OPPOSITE SIDE? 23,78,5

THE THIRD ANGLE IS 79 DEGREES AND THE TWO UNKNOWN OPPOSITE SIDES ARE 12.5169 AND 12.5614.

## Two Sides, Included Angle Program

- 5 '2 SIDES, INCLUDED ANGLE
- 10 CLS
- 20 INPUT"ENTER THE TWO SIDES (A,B) AND THE INCLUDED ANGLE"; AS, BS, CA
- 30 CS=SQR(AS+2+BS+2-(2\*AS\*BS\*COS(C A/57.29578)))
- 40 AA=ATN(AS\*SIN(CA/57.29578)/CS/S QR(-AS\*SIN(CA/57.29578)/CS\*AS\*S IN(CA/57.29578)/CS+1))
- 50 AA=AA\*57.29578
- 60 BA=180-AA-CA
- 70 PRINT"THE THIRD SIDE IS"CS"."CH R\$(13)"THE CORRESPONDING ANGLES FOR THE TWO KNOWN SIDES ARE"AA CHR\$(13)"AND"BA"DEGREES."

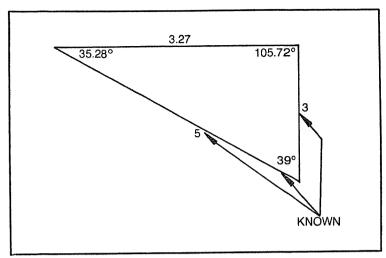


Fig. 5-16. A triangle with two known sides, included angle.

## Two Sides, Included Angle Example

Solve Fig. 5-16 for the unknown side and angles.

ENTER THE TWO SIDES (A,B) AND THE INCLUDED ANGLE?

?3,5,39

THE THIRD SIDE IS 3.26889.

THE CORRESPONDING ANGLES FOR THE TWO KNOWN SIDES ARE 35.2787 AND 105.721 DEGREES.

## **GREAT CIRCLE CALCULATIONS**

The last program in this chapter will compute the distance in nautical miles and bearing (referenced to True North) between two points on the Earth. Information for this program must be entered as decimal degrees. Plus, Southern Latitudes and Eastern Longitudes must be entered as negative numbers.

The equations to manually calculate the distance and bearing are:

A = 
$$(\sin \text{LA1} \cdot \sin \text{LAZ} + \cos \text{COS} \text{LA1} \cdot \cos \text{LAZ} \cdot \cos \text{(LO2-LO1)})$$
  
D =  $60 \cdot \cos^{-1} A$ 

$$C = \frac{\sin \text{LA2} - (\sin \text{LA1} \cos \text{D/60})}{\sin (\text{D/60}) \cos \text{LA1}}$$

$$H = \cos^{-1}C$$

```
329)*COS(LA(2)*.01745329)*COS((LO(2)-LO(1))*.01745329)
80 D=60*(-ATN(A/SQR(-A*A+1))+1.5708)*57.29579
90 C=(SIN(LA(2)*.01745329)-(SIN(LA(1)*.01745329)*COS(D/60*.01745329)))/(SIN(D/60*.01745329)*COS(LA(1)*.01745329))
100 H=(-ATN(C/SQR(-C*C+1))+1.5708)*57.29579
110 F=SIN(LO(2)-LO(1))
120 IF F>=0 H=360-H
                                                                                                                                                                                                                                                                                                                                                                            A=SIN(LA(1)*,01745329)*SIN(LA(2)*,01745329)+COS(LA(1)*,01745
PRINT"WHEN ENTERING DATA, SOUTHERN LATITUDES AND EASTERN LONGITUDES MUST BE ENTERED AS NEGATIVE NUMBERS."
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    PRINT" THE DISTANCE IS"D"NAUTICAL MILES AT A BEARING OF "H"DEGREES."
                                                                                                       PRINT"ENTER LATITUDE AND LONGITUDE (1AT, 10N) OF THE
                                                                                                                                                                                                                                           PRINT"ENTER LATITUDE AND LONGITUDE (LAT, LON) OF THE
                                                                                                                                                                                                                                                                            DESTINATION"
INPUT LA(2), LO(2)
                                                                                                                                            STARTING POINT INPUT LA(1), LO(1)
                                                                              PRINT
                                                                                                                                                                                    0 †
```

5 'gREAT CIRCLE

**Great Circle Program** 

## **Great Circle Example**

Compute the great circle distance and bearing from San Francisco to Tokoyo.

	Latitude	Longitude
San Francisco	37.82 N	122.42 W
Tokoyo	35.67 N	139.75 E

WHEN ENTERING DATA, SOUTHERN LATITUDES AND EASTERN LONGITUDES MUST BE ENTERED AS NEGATIVE NUMBERS.

ENTER LATITUDE AND LONGITUDE (LAT, LON) OF THE STARTING POINT

? 37.82, 122.42

ENTER LATITUDE AND LONGITUDE (LAT, LON) OF THE DESTINATION

? 35.67, -139.75

THE DISTANCE IS 4456.89 NAUTICAL MILES AT A BEARING OF

303.292 DEGREES.

Again note that the Eastern Longitude of Tokoyo was entered as a negative number.



## Appendix A Statements and Commands in BASIC

**AUTO** 

CLEAR

CLEAR N

CLOAD

CLOAD?

turn on automatic line numbering. Can be set for different increments. set numerics to zero, strings to null. same as CLEAR but sets aside a certain amount of memory for strings (N). load program from cassette player. If no file-name is specified, the current program will be loaded. compares program on tape

with program in memory. If programs are not equal "BAD" will be printed on video display.

CONT continue after BREAK or

STOP in execution.

CSAVE saves current program on

cassette tape, a file-name should be used so that

program can be compared

with what is in memory.

DATA hold DATA for accessby

READ statement.

DELETE delete program line or lines

specified by INPUT

statement.

DIM allocate storage for dimen-

sional array with specified

size per dimension.

EDIT puts computer in EDIT

mode for line specified.

END end execution of program,

returns computer to

command mode.

ERROR if an error is encountered

in the program, the computer prints the offending line number and the error

code for that line.

FOR—TO- open a FOR-NEXT loop.

FOR—TO-STEP— open a FOR-NEXT loop

with optional STEP. If no step is specified an incre-

ment of one is used.

GOTO branch to a specified line

number in the program.

GOSUB branch to a sub-routine

beginning with the speci-

fied line number.

IF-THEN-ELSE test expression; if true,

execute the statement and jump to the next program line. If it's false, the ELSE

statement will be executed.

INPUT await input from keyboard.

INPUT #-1 input from cassette #1. LET (var-exp) assigns the value of an ex-

pression to variable. The LET is optional with LEVEL

II BASIC.

LIST list all program lines, or a

specified range of lines.

NEXT var. close the FOR - NEXT loop.

The variable may be omitted, or a variable list may be used to close

nested loops.

NEW deletes the entire program

in memory and returns to command mode.

ON-GOTO branches to a specified

line number after

evaluating the expression. Otherwise go to the next

statement.

ON-GOSUB same as ON - GOTO but

branches to the appropriate

GOSUB statement.

PRINT exp.

RESTORE

outputs to the video display the value of exp, which can be a string expression,

a numeric, a constant or a

list of items.

PRINT #-1 output to cassette #1
PRINT begins printing at a

specified area on the video display; a PRINT modifier.

PRINT USING PRINT format specifier, out-

put exp in a form

specified by a string field.

RANDOM reseeds the RANDOM

number generator.

REM remark indicator. The rest

of line is ignored.

READ assigns values to specified

variables starting with

the current DATA element. resets the data pointer to

the first item in the first

DATA statement.

RESUME returns from the error

routine to the line specified.

RETURN branch statement following

last GOSUB executed.

RUN execute the program. If no

line is specified, execution begins with the program's

lowest line number.

STOP stop the program's exe-

cution and print a break message containing current line number. Program execution can resume with CONT.

**SYSTEM** 

enter the monitor code for loading a machine language program from cas-

sette tape player.

TAB

print modifier; begins printing at specified TAB area of the video display.

TROFF

turn off the line-numbers

trace.

**TRON** 

turn on the line numbers trace (very useful when debugging).

## **String Functions**

ASC

returns the ASCII code of first character in string

argument.

CHR\$

returns a one-character string defined by a code.

If a contol function is

specified by code,

that function is acti-vated.

FRE

returns amount of memory available for string storage.

**INKEY\$** 

strobes the keyboard and

returns a one-character string corresponding to the key pressed during

strobe.

LEN returns the numeric

length of string.

LEFT\$ returns the first n

characters of a string (when n is a numeric

expression).

MID\$ returns the substring of a

string with length n and

starting at position

MID\$ (cont) minastring (wheren and m

are numeric expressions).

RIGHT\$ returns the last n

characters of a string (where n is a numeric

expression).

STR\$ returns a string

representation of an

evaluated argument.

STRING\$ returns a sequence of char-

acters using the first character. PRINTSTRINGS\$ (50, "\*"), for example, will print 50 asterisks on the

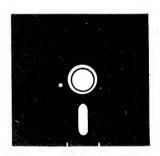
video display.

VAL returns a numeric value

corresponding to a

numeric-valued string, such

as PRINT VAL (A\$+W\$).



## Appendix B Powers of Two

n	2ª	2" THREE BYTE BINARY
0	1	00000000 00000000 00000001
1	2	00000000 00000000 00000010
2	4	00000000 00000000 00000100
3	8	00000000 00000000 00001000
4	16	00000000 00000000 00010000
5	32	00000000 00000000 00100000
6	64	00000000 00000000 01000000
4 5 6 7	128	00000000 00000000 10000000
8	256	00000000 00000001 00000000
9	512	00000000 00000010 00000000
10	1024	00000000 00000100 00000000
11	2048	00000000 00001000 00000000
12	4096	00000000 00010000 00000000
13	8192	00000000 00100000 00000000
14	16384	00000000 01000000 00000000
15	32768	00000000 10000000 00000000
16	65536	00000001 00000000 00000000
17	131072	00000010 00000000 00000000
18	262144	00000100 00000000 00000000
19	524288	00001000 00000000 00000000
20	1048576	00010000 00000000 00000000
21	2097152	00100000 00000000 00000000
22	4194304	01000000 00000000 000000000
23	8388608	10000000 00000000 00000000

## Appendix C Hexadecimal-Decimal Integer Conversion



The following table provides for direct conversions between hexadecimal integers in the range 0-FFF and decimal integers in the range 0-4095. For conversion of larger integers, the table values may be added to the following figures:

Hexadecimal	Decimal	Hexadecimal	Decimal
01 000	4 0%	20 000	131 072
02 000	8 192	30 000	196 608
03 000	12 288	40 000	262 144
04 000	16 384	50 000	327 680
<b>0</b> 5 000	20 480	60 000	393 216
06 000	24 576	70 000	458 752
07 000	28 672	80 000	524 288
08 000	32 76 <b>8</b>	90 000	589 824
09 000	36 864	A0 000	655 360
<b>0</b> A 000	40 960	BO 000	720 896
OB 000	45 056	C0 000	786 432
<b>0</b> C 000	49 152	DO 000	851 968
0D 000	53 248	E0 000	917 504
OE 000	57 344	FO 000	983 040
<b>0</b> F 000	61 440	100 000	1 048 576
10 000	65 536	200 000	2 097 152
11 000	69 632	300 000	3 145 728
12 000	<b>73</b> 728	400 000	4 194 304
13 000	77 824	500 000	5 242 880
14 000	81 920	600 000	6 291 456
15 000	86 01 <b>6</b>	<b>7</b> 00 000	7 340 032
16 000	90 112	800 0 <b>00</b>	8 388 608
17 000	94 208	900 000	9 437 184
18 000	98 304	A00 000	10 485 760
19 000	102 400	B00 000	11 534 336
1A 000	106 496	C00 000	12 582 912
1B 000	110 592	D00 000	13 631 488
IC 000	114 688	E00 000	14 680 064
1D 000	118 784	F00 000	15 728 640
1E 000	122 880	1 000 000	16 777 216
1F 000	126 976	2 000 000	33 554 432

## HEXADECIMAL-DECIMAL INTEGER CONVERSION

	٥	-	2	2	4	5	0	7	8	٥	4	8	U	۵	E	ш
88	0000	500	0000	0003	900	5000	9000	0007	8008	6000	0000	0011	0012	0013	9014	0015
200	0032	0033	0034	0035	0039	0037	0038	0039	0040	8 2	0042	0043	0044	8645	868	86.2
030	0048	9043	0020	0051	0052	0053	0054	0055	9056	00057	0058	6500	0900	900	000	000
S	0064	0065	900	2900	0063	6900	0070	1/00	0072	0073	0074	0075	9200	7/00	8/00	6/00
050	0800	0081	0082	0083	9084	0085	9800	0087	0088	6800	0000	<u>1600</u>	0005	0093	0094	90095
980	9500	2600	8600	6600	0010	0101	0102	0103	90	0105	910	0107	0108	010	01 10	===
070	0112	0113	0114	0115	9110	2110	0118	6110	0150	0121	0122	0123	0124	0125	0126	0127
80	0128	0129	0130	0131	0132	0133	0134	0135	0138	0137	0138	0139	0140	0141	0142	0143
0%0	0144	0145	0146	0147	0148	0149	0150	0151	0152	0153	0154	0155	0156	0157	0.58	0159
040	0100	1910	0162	0163	0164	0165	9910	2910	9910	6910	0170	0171	0172	0173	0174	0175
080	0176	0177	9178	0179	0180	0181	0182	0183	0184	0185	918	0187	0188	0189	0180	1610
					į						0	0	000	000	6	2000
ပ္တ	0192	0193	0194	0195	0196	200	9610	0199	0200	020	2020	0703	0,00	020	0206	020
3 5	0208	0209	277	1170	0220	0220	0220	223	0230	220	0223	0235	22.5	0237	0238	0230
9 6	0240	0241	0220	0243	0243	0245	0246	0247	0248	0249	0220	0251	0.52	0253	0254	0255
2	2		7470	2570	70	2	2	770								

					**************************************
0271 0287 0303 0319	0335 0351 0367 0383	0399 0415 0431	0463 0479 0495 0511	0527 0543 0559 0575	0591 0607 0623 0639
0270	0334	0398	046 <b>2</b>	0526	0590
0286	0350	0414	0478	0542	0606
0362	0366	0430	0494	0558	0622
0318	0382	0446	0510	0574	0633
0269	0333	0397	0461	0525	0589
0285	0349	0413	0477	0541	0605
0301	0365	0429	0493	0557	0621
0317	0381	0445	0509	0573	0637
0263	0332	0396	0460	0524	0588
0284	0348	0412	0476	0540	0604
0300	0364	0423	0492	0556	0620
0316	0380	0444	0508	0572	0638
026 <b>7</b>	0331	0395	0459	0523	0587
0283	0347	0411	0475	0539	0603
0299	0363	0427	0491	055 <b>5</b>	0619
031 <b>5</b>	0379	0443	050 <b>7</b>	0571	0635
0266	0330	0394	0458	0522	0586
0282	0346	0410	9474	0538	0602
0298	0362	0426	0490	0554	0618
0314	0378	0442	050 <b>6</b>	0570	0634
0265	0329	0393	0457	0521	0585
0281	0345	0409	0473	0537	0601
0297	0361	0425	0489	0553	0617
0313	0377	0441	0505	0569	0633
0264	0328	03%2	<b>04</b> 56	0520	058 <b>4</b>
0280	0344	0408	0472	0536	0600
0236	0360	0424	0488	0552	0616
0312	0376	<b>0</b> 440	0504	0552	0632
0263	0327	0391	0455	0519	0583
0279	0343	0407	0471	0535	0599
0295	0359	0423	0487	0551	0615
0311	0375	0439	0503	0567	0631
0262	0326	03%	0454	0518	0582
0278	0342	0408	0470	0534	0598
0294	0358	0422	0486	0550	0614
0310	0374	0438	0502	0566	0630
0261	0325	0389	0453	0517	0581
0277	0341	0405	0469	0533	0597
0293	0357	0421	0485	0549	0613
0309	0373	0437	0501	0565	0629
0260	0324	0388	0452	0516	0580
0276	0340	0404	0468	0532	0596
0292	0356	0420	0484	0548	0612
0308	0372	<b>0</b> 43 <b>6</b>	0500	0564	0628
025 <b>9</b>	0323	0387	0451	051 <b>5</b>	057 <b>9</b>
027 <b>5</b>	0339	0403	0467	0531	0595
029 <b>1</b>	0355	0419	0483	0547	0611
030 <b>7</b>	0371	0435	0499	0563	0627
0259	0322	0388	0450	0514	0578
0274	0338	0402	0466	0530	0594
0290	0354	0418	0482	0546	0610
030 <b>6</b>	0370	0434	0498	0562	0626
0257	0321	0385	0449	0513	0577
0273	0337	0401	0465	0529	0593
0289	0353	0417	0481	0545	0609
0305	0369	0433	0497	0561	0625
0256	0320	0384	044 <b>8</b>	0512	057 <b>6</b>
0272	0336	0400	0464	0528	0592
0288	0352	0416	0480	0544	0608
0304	0368	0432	049 <b>6</b>	0560	0624
30 22 28	140 150 170	8 5 2 8 8 2 8 8	<u> </u>	200 210 220 230	240 250 260 270

# HEXADECIMAL-DECIMAL INTEGER CONVERSION (continued)

u_	0655 0671 0637 0637 0703	0719 0735 0751 0751	0783 0799 0815 0815	0847 0863 0879 0895	0911 0927 0943 0959	0975 0991 1007 1023
E	0654	0718	0782	0846	0910	0974
	0670	0734	0798	0862	0926	0990
	0686	0750	0814	0878	0942	1006
	0702	0766	0830	0894	0958	1022
۵	0653	0717	0781	0845	0909	0973
	0669	0733	0797	0861	0925	0989
	0685	0749	0813	0877	0941	1005
	0701	0765	0829	0893	0957	1021
U	0652	0716	0780	0844	0908	0972
	0668	0732	0796	0860	0924	0988
	0684	0748	0812	0876	0940	1004
	0700	0764	0828	0892	0956	1020
8	0651	0715	0779	0843	0907	0971
	0667	0731	0795	0859	0923	0987
	0683	0747	0311	0875	0939	1003
	0699	0763	0827	0891	0955	1019
∢	0550	0714	0778	0842	090 <del>6</del>	0970
	0666	0730	0794	0858	0922	0966
	0682	0746	0810	0874	0938	1002
	0698	0762	0826	0890	0954	1013
٥	064 <b>9</b>	0713	0777	0841	0905	0969
	0665	0729	0793	0857	0921	0985
	0681	0745	0809	0873	0937	1001
	0697	0761	0825	0889	095 <b>3</b>	1012
8	0648	0712	0776	0840	0904	0968
	0680	0728	0792	0856	0920	0984
	0690	0744	0808	0872	0926	1000
	0696	0760	0824	0888	0952	1016
^	0647	0711	0775	0839	0903	0967
	0663	0727	0791	0855	0919	0983
	0679	0743	0807	0871	0915	0999
	0695	0759	0823	0887	0951	1015
9	0646	07 10	0774	0838	0902	0966
	0662	07 26	0790	0854	0918	0982
	0678	07 42	0806	0570	0914	0998
	0678	07 58	0822	0886	0950	1014
5	0645	0709	0773	0837	0901	0965
	0661	0725	0789	0853	0917	0981
	0677	0741	0805	0869	0913	0997
	0693	0757	C821	0885	0949	1013
4	0644	0708	0772	0836	0900	0964
	0660	0724	0788	0852	0916	0980
	0676	0740	0904	0363	0912	0996
	0678	G756	0820	0884	0946	1012
9	0643	0707	0771	0835	0839	0963
	0659	0723	0787	0851	0935	0979
	0675	0739	0803	0867	0931	0995
	0691	0755	0819	0863	0947	1011
2	06.42	07C6	07.70	0850	0858	0952
	06.53	0722	07.86	0850	0934	0978
	06.74	0738	0802	0866	0530	0994
	06.70	0754	0818	0882	0946	1010
-	0641	0705	0769	0333	0897	0961
	0657	0721	0785	0849	0933	0977
	0673	0737	0601	0355	0927	0993
	0689	0753	0817	0881	0927	1009
0	0640	0704	0768	0832	0896	0960
	0656	0720	0784	0643	0932	0976
	0672	0730	0300	0864	0928	0992
	0688	0752	0816	0860	0944	1008
<b></b>	280 290 2A0 280	2C0 2D0 2E0 2F0	300 310 320 330	340 350 360 370	380 390 380	3C0 3E0 3F0

1039 1055 1071	1103 1119 1135 1151	1167 1183 1199 1215	1231 1247 1263 1279	1295 1311 1327 1343	1359 1375 1391 1407
1038	1102	1166	1230	1294	1358
1054	1118	1182	1246	1310	1374
1070	1134	1198	1262	1326	1390
1086	1150	1214	1262	1342	1406
1037	1101	1165	1229	1293	1357
1053	1117	1191	1245	1309	1373
1069	1133	1197	1261	1325	1389
1085	1149	1213	1277	1341	1405
1036	1100	1164	1228	1292	1356
1052	1116	1180	1244	1308	1372
1068	1132	1196	1260	1324	1388
1084	1148	1212	1276	1340	1404
1035	1099	1163	1227	1291	1355
1051	1115	1179	1243	1307	1371
1067	1131	1195	1259	1323	1387
1083	1147	1211	1275	1339	1402
1034	1098	1162	1226	1290	1354
1050	1114	1178	1242	1306	1370
1066	1130	1194	1258	1322	1386
1082	1146	1210	1258	1338	1402
1033	1097	1161	1225	1289	1353
104 <b>?</b>	1113	1177	1241	1305	1369
1065	1129	1193	1257	1321	1385
1081	1145	1209	1257	1337	1401
1032	1096	1160	1224	1288	1352
1048	1112	1176	1240	1304	1368
1064	1128	1192	1256	1320	1384
1080	1144	1208	1272	1336	1400
1031	1095	1159	1223	1287	1351
1047	1111	1175	1239	1303	1367
1063	1127	1191	1255	1319	1383
1079	1143	1207	1251	1335	1399
1030	1094	1158	1222	1286	1350
1046	1110	1174	1238	1302	1366
1062	1126	1190	1254	1318	1382
1078	1142	1206	1270	1334	1398
102 <b>9</b>	1093	1157	1221	1285	1349
1045	1109	1173	1237	1301	1365
1061	1125	1189	1253	1317	1381
1077	1141	1205	1269	1333	1397
1028	1092	1156	1220	1284	1348
1044	1108	1172	1236	1300	1364
1060	1124	1188	1252	1315	1380
1076	1140	1204	1252	1322	1396
1027	1091	1155	1219	1283	1347
1043	1107	1171	1235	1299	1363
1059	1123	1187	1251	1315	1379
1075	1139	1203	1267	1331	1395
1026	1090	1154	1218 .	1282	1346
1042	1106	1170	1234	1298	1362
1058	1122	1186	1250	1314	1378
1074	1138	1202	1266	1330	1394
1025	1089	1153	1217	1281	1345
1041	1105	1169	1233	1297	1361
1057	1121	1185	1249	1313	1377
1073	1137	1201	1265	1329	1393
1024	1088	1152	1216	1280	1344
1040	1104	1168	1232	1296	1360
1056	1120	1184	1243	1312	1376
1072	1136	1200	1264	1328	1392
400	440	480	4C0	500	540
410	450	490	4D0	510	550
420	460	4A0	4F0	520	560
430	470	480	4F0	530	570

HEXADECIMAL-DECIMAL INTEGER CONVERSION (continued)

							_									-					an magazine		-		
ų	-	1423	1439	1455	1471	1487	1503	1519	1535	1551	1567	1583	1599	1615	1631	1647	1663	1679	1695	17.	1727	1743	1759	1775	<u> </u>
,	.	1422	1438	1454	1470	1486	1502	1518	1534	1550	1566	1582	1593	1614	1630	1645	1652	1678	1694	1710	1726	1742	1758	1774	<u>}</u>
,	۱ء	1421	1437	1453	1469	1485	1501	1517	1533	1549	1565	1531	1597	1613	1629	1645	2 20	1677	1693	1709	1725	1741	1757	1773	1/89
,	١	1420	1436	1452	1468	1484	1500	1516	1532	1548	1564	1580	15%	1612	1628	1644	099	1675	1692	1798	1724	1740	1756	1772	1/88
	ا ۵	419	435	451	1467	1483	499	1515	1531	1547	1563	1579	1595	1611	1627	16/3	1659	1675	1691	1707	1723	1730	1755	1771	1787
	◄	1418	1434	1450	1466	1482	1498	1514	1530	1546	1562	1578	1594	1610	1626	0701	1658	1674	1690	1706	1722	1738	1754	1770	1786
	٥	1417	1433	1449	1465	1481	1497	1513	1529	1545	1561	1577	1593	1600	1625	107	1657	1673	1682	1705	1721	1737	1753	1769	1785
	œ	1416	1432	1448	1464	1480	14%	1512	1528	1544	1560	1576	1592	1600	1624	100	1656	1672	1688	1704	1720	4726	1752	1768	1784
	7	1415	1431	1447	1463	1479	1405	1511	1527	1543	1559	1575	1531	1407	200	507	1655	1671	1687	1703	6121	3621	3 2	1767	1783
	Ŷ	1414	1430	1446	1462	1478	1494	1510	1526	1542	1558	1574	1590	707.	1422	7701	1654 1654	1670	1686	1702	1718		1750	266	1782
	2	1413	1429	1445	146	1477	1493	1509	1525	1541	1557	1573	1589	30.7	000	1701	53 53	1440	1685	1707	1717		1740	1765	1781
	₹	1412	1428	1444	1460	1476	1492	1508	1524	1540	15.56	1572	1588	3	20.5	0701	1636	8771	1684	202	1716		17.40	1764	1780
	ب ص	1411	1427	1443	1459	7.5	1071	1507	1523	1530	1555	155	1587		200	610	1035 1651		1662	1600	1715		1731	1763	1779
	2	1410	1426	1442	1458	1474	8	1506	1522	1528	1554	1570	1586		7091	9	1634 1650		1666	7991 1698	1714		1730	1746	1778
		1409	1425	1441	1457	1473	0871	1505	1521	1537	1557	15.00	1585	;	9	121	1633 1643		1665	1601	1713		1729	1745	1777
	0	1408	1424	1440	1455	1473	1,459	1504	1520	1636	1550	1640	584		0091	9191	1532		1664	1606	1712		1728	1744	1776
		580	8	5A0	580	0	2 2	3 5	5.5	Ş	3 5	0.0	970		940	650	670	) ;	089	26	680		00 00 00	009	6F0
														THE PERSON NAMED IN	مبجله	-	58 20 mm	Marie Const						-	

1807	1871	1935	1999	2063	2127
1823	1887	1951	2015	2079	2143
1839	1903	1967	2031	2095	2159
1855	1919	1983	2047	2111	2175
1806	1870	1934	1998	2062	2126
1822	1836	1950	2014	2078	2142
1838	1902	1966	2030	2094	2158
1854	1918	1982	2046	2110	2158
1805	1869	1933	1997	2061	2125
1821	1885	1949	2013	2077	2141
1837	1901	1965	2029	2093	2157
1853	1917	1981	2045	2109	2173
1804	1868	1932	1996	2060	2124
1820	1884	1948	2012	2076	2140
1836	1900	1964	2026	2092	2156
1852	1916	1980	2044	2108	2172
1803	1867	1931	1995	205 <b>9</b>	2123
1819	1883	1947	2011	207 <b>5</b>	2139
1835	1899	1963	2027	2091	2155
1851	1915	1979	2043	210 <b>7</b>	2151
1802	1866	1930	1994	2058	2122
1818	1882	1946	2010	2074	2138
1834	1898	1962	2026	2090	2154
1850	1914	1978	2042	2106	2150
1801	1865	1929	1993	2057	2121
1817	1881	1945	2009	2073	2137
1833	1897	1961	2025	2069	2153
1849	1913	1977	2041	2105	2153
1800	1864	1928	1992	2056	2120
1816	1880	1944	2008	2072	2138
1832	1896	1960	2024	2088	2152
1848	1912	1976	2040	2104	2158
1799	1863	1927	1991	2055	2119
1815	1879	1943	2007	2071	2135
1831	1895	1959	2023	2087	2151
1847	1911	1975	2039	2103	2167
1798	1862	1926	19%0	2054	2118
1814	1878	1942	2006	2070	2134
1830	1894	1958	2022	2086	2150
1846	1910	1974	2033	2102	2166
1797	1861	1925	1989	2053	2117
1813	1877	1941	2005	2069	2133
1829	1893	1957	2021	2085	214.7
1845	1909	1973	2037	2101	2165
1796	1860	1924	1988	2052	21.16
1812	1876	1940	2004	2068	2132
1828	1892	1956	2020	2084	2148
1844	1908	1972	2036	2100	2164
1795	185 <b>9</b>	1923	1987	2051	2115
1811	1875	1939	2003	2067	2131
1827	1891	1955	2019	2083	2147
1843	1907	1971	2035	2099	2163
1794	1858	1922	1986	2050	2114
1810	1674	1938	2002	2066	2130
1826	1890	1954	2018	2082	2146
1842	1906	1970	2034	2098	2152
1793	1857	1921	1985	2049	2113
1809	1873	1937	2001	2065	2129
1825	1889	1953	2017	2081	2145
1841	1905	1969	2033	2097	2145
1792	1856	1920	1984	2048	2112
1808	1872	1935	2000	2064	2128
1824	1888	1952	2016	2080	2144
1840	1904	1968	2032	2096	2160
730	740	780	700	800	840
710	750	790	700	810	850
720	760	7A0	760	820	860
730	770	780	770	830	870

HEXADECIMAL-DECIMAL INTEGER CONVERSION (continued)

The second secon					
2191	2255	2319	2383	2447	2511
2207	2271	2335	2399	2463	2527
2223	2287	2351	2415	2479	2543
2239	2303	2367	2431	2495	2559
21%	2254	2334	2332	2446	2510
220%	2270	2334	23%	2462	2526
2222	2236	2350	2414	2478	2542
2238	2302	2356	2430	2494	2558
2189	2253	2317	2331	2445	2509
2205	2269	2333	2397	2461	2525
2221	2285	2349	2413	2477	2541
2237	2301	2365	2429	2493	2557
2188	2252	2316	2380	2444	2508
2204	2268	2332	2396	2460	2524
2220	2284	2348	2412	2476	2540
2236	2300	2348	2428	2492	2556
2167	2251	2315	2379	2443	2507
2203	2267	2331	2395	2459	2523
2219	2283	2347	2411	2475	2539
2235	2299	2363	2427	2491	2555
2186	2250	2314	2378	2442	2506
2202	2266	2330	2394	2458	2522
2218	2282	2346	2410	2474	2538
2218	2298	2362	2426	2490	2554
2185	224 <b>9</b>	2313	2377	2441	2505
2201	2265	2329	2393	2457	2521
2217	2281	2345	2409	2473	2537
2233	2297	2361	2425	2489	2553
2184	2248	231 <b>2</b>	2376	2440	2504
2260	2264	2328	2392	2456	2520
2216	2280	2344	2468	2472	2535
2232	2296	2360	2424	2488	2552
2183	2247	2311	2375	2439	2503
2199	2263	2327	2391	2455	2519
2215	2279	2343	2307	2471	2535
2231	2295	2359	2423	2487	2551
2182	2246	2310	2374	2438	2502
2198	2262	2326	2390	2454	2518
2214	2278	2342	2406	2470	2534
2230	2294	2358	2422	2486	2550
2181	2245	2309	2373	2437	2501
2157	2261	2325	2389	2453	2517
2213	2277	2341	2405	2469	2533
2229	2293	2357	2421	2485	2549
2180	2244	2308	2372	2436	2500
2196	2260	2324	2383	2452	2516
2212	2276	2340	2404	2468	2532
2228	2292	2356	2420	2484	2548
2179	2243	2307	2371	2435	2499
2195	2259	2323	2387	2451	2515
2211	2275	2339	2403	2467	2531
2227	2291	2355	2419	2483	2547
2178	2242	2306	2370	2434	24%
2194	2258	2322	2386	2450	2514
2210	2274	2333	2402	2466	2530
2226	2290	2354	2418	2482	2546
2177	2241	2305	2369	2433	2497
2193	2257	2321	2385	2449	2513
2209	2273	2337	2401	2465	2529
2225	2259	235 <b>3</b>	2417	2481	2545
2176	2240	2304	2368	2432	2495
2192	2256	2320	2384	2448	2512
2208	2272	2336	2400	2464	2526
2224	2288	2352	2416	2480	2544
880	8C0	900	940	980	%0
890	8D0	910	950	990	%0
8A0	8E0	920	950	9A0	%0
8B0	8F0	930	970	980	%0
	2176         2177         2178         2179         2180         2181         2183         2184         2185         2186         2167         2189         2190         2190         2200         2201         2202         2203         2204         2205         2206         2206         2206         2207         2203         2204         2205         2206         2203         2204         2205         2206         2203         2204         2205         2206         2203         2204         2205         2206         2203         2204         2205         2206         2203         2204         2205         2207         2203         2204         2205         2202         2203         2204         2205         2202         2203 <th< th=""><th>2176         2177         2178         2179         2180         2181         2183         2184         2185         2186         2187         2189         2199         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2204         2205         2203         2204         2205         2203         2204         2205         2203         2204         2205         2217         2218         2219         2220         2221         2221         2217         2218         2219         2220         2220         2221         2221         2217         2218         2219         2220         2221         2221         2221         2217         2218         2219         2220         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2222         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         <th< th=""><th>2176         2177         2178         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  2183         2184         2187         2189         2189         2180         2197         2188         2189         2180         2190         2200         2201         2202         2203         2204         2205         2216         2217         2218         2219         2219         2210         <th< th=""><th>2176         2177         2178         2179         2180         2181         2182         2183         2184         2185         2186         2179         2193         2194         2179         2193         2194         2195         2194         2195         2196         2197         2193         2194         2195         2196         2197         2193         2194         2195         2196         2197         2193         2204         2205         2203         2204         2205         2203         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205     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 2204         2205         2203         2204         2205         2217         2218         2219         2220         2221         2221         2217         2218         2219         2220         2220         2221         2221         2217         2218         2219         2220         2221         2221         2221         2217         2218         2219         2220         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2221         2222         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234         2234 <th< th=""><th>2176         2177         2178         2179         2180         2181         2184         2184         2185         2186         2187         2189         2189         2189         2189         2189         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2190         2200         2201         2202         2203         2203         2204         2203         2214         2215         2216         2217         2218         2219         2200         2201         2202         2203         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         <th< th=""><th>2176         2179         2179         2180         2181         2182         2183         2184         2185         2186         2170         2170         2177         2178         2179         2180         2180         2181         2183         2184         2187         2189         2189         2180         2197         2188         2189         2180         2190         2200         2201         2202         2203         2204         2205         2216         2217         2218         2219         2219         2210         <th< th=""><th>2176         2177         2178         2179         2180         2181         2182         2183         2184         2185         2186         2179         2193         2194         2179         2193         2194         2195         2194         2195         2196         2197         2193         2194         2195         2196         2197         2193         2194         2195         2196         2197         2193         2204         2205         2203         2204         2205         2203         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2206         2207         2204         2205         2204         2205         2204         2205         2204         2205       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2197         2193         2194         2195         2196         2197         2193         2194         2195         2196         2197         2193         2204         2205         2203         2204         2205         2203         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2206         2207         2204         2205         2204         2205         2204         2205         2204         2205         2204         2205         2206         2207         2208         2207         2208         2204         2205         2206         2207         2206         2206         2207         2206         2207         2208         2206         2207         2208         2206         2206         2206         2206         2206         <th< th=""></th<></th></th<></th></th<>	2176         2179         2179        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# MEXADECIMAL-DECIMAL INTEGER CONVERSION (continued)

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	2974	3038	3102	3166	3230	3294
	2990	3054	3118	3182	3246	3310
	3006	3070	3134	3198	3262	3326
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	2973	3037	3101	3165	3229	3293
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	2972	3035	3100	3164	3228	3292
	2988	3052	31 i 6	3180	3244	3308
	3004	3068	3132	3196	3260	3324
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	3003	3067	3131	1195	1259	332 <b>3</b>
4	2954 2 2970 2 2986 2 3002 3	3018 3 3034 3 3050 3	3098 3 3098 3 3114 3	3146 3 3162 3 3178 3 3194 3	3226 3 3226 3 3242 3 3258 3	3274 3 3290 3 3306 3 3322 3
		(3 (3 (3 (3	(7 (7 (7 (7	()()()()	6,6,6,6,6	0,0,0,0
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	2969	3033	3097	3151	3225	3289
	2985	3049	3113	3177	3241	3305
	3001	3065	3129	3193	3257	3321
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	3000	3064	3128	3192	3256	3320
_	2951	3015	3079	3143	3207	3271
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	2983	3047	3111	3175	3239	3303
	2999	3063	3127	3191	3255	3319
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	963	8027	3091	3155	3219	3283
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	8995	8059	3123	3187	3251	3315
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	2962	3026	3090	3154	3218	3282
	2978	3042	3106	3170	3234	3273
	2994	3058	3122	3186	3250	3314
-	2945	3009	3073	3137	320	3265
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	2993	3057	3121	3185	3249	3313
0	2944	3008	3072	3136	3200	3264
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	2976	3040	3104	3168	3232	3296
	2992	3056	3120	3184	<b>3</b> 248	3312
Limit	880 890 8A0 880	8C0 8D0 8E0 8F0	8228	020 020 020 020 020	80008 8008 8008	888 <b>8</b>

m @ 10 ==	> m m ::			0.0	
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337 <b>3</b>	3437	3501	3565	3629	3693
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3386	3450	3514	3562	3642	3706
3337	3401	3465	3529	3593	3657
3353	3417	3481	3545	3609	3673
3369	3433	3497	3561	3625	3689
3385	3449	3513	3577	3641	3705
3336 3352 3368 3384	3400 3416 3448	3464 3480 34% 3512	3528 3544 3560 357 <b>6</b>	3592 3608 3624 3640	365 <b>6</b> 367 <b>2</b> 3688 3704
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3383	3447	3511	3559	3639	3703
3334 3350 3366 3382	3338 3414 3446	3462 3478 3494 3510	3526 3542 3558 3574	3590 3606 3622 3638	3654 3670 3686 3702
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3365	3429	3493	3557	3621	3685
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3332	33%	3460	3524	3588	3652
3348	3412	3476	3540	3604	3668
3364	3428	3492	3556	3620	3684
3380	3444	3508	3572	3636	3700
3331	3395	345 <b>9</b>	3523	3587	3651
3347	3411	347 <b>5</b>	3539	3603	3667
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3328	3392	3456	3520	3584	3648
3344	3408	3472	3536	3600	3564
3360	3424	3488	3552	3615	3680
3376	3440	3504	3552	3632	3696
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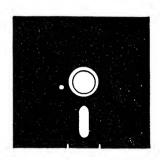
HEXADECIMAL-DECIMAL INTEGER CONVERSION (continued)

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												0	7010	1000	2020	4040
E80	3712		3714	1715	3716	3717	3718	3719	3720	3/21	3/55	3/53	3/24	3/23	07/50	27.57
8	3728		3730	3731	3732	3733	3734	3735	3736	3737	3738	3739	3740	3/41	3/42	3/43
FAO	3744		3746	3747	3748	3749	3750	3751	3752	3753	3754	3755	3756	3757	3758	3759
88	3760	3761	3762	3763	3764	3765	3766	3767	3768	3769	3770	3771	3772	3773	3774	3775
2	3776				3780	3781	3782	3783	3784	3785	3786	3787	3788	3789	3790	3791
2	3702				3796	3797	3798	3799	3800	3801	3802	3803	3804	3805	3806	3807
3 4	3808				3812	3813	3814	3815	3816	3817	3818	3819	3820	3821	3822	3823
100	3824				3828	3829	3830	3831	3832	3833	3834	3835	3836	3837	3838	3839
2 5	2040	30.11			3844	3845	3846	3847	3848	3849	3850	3851	3852	3853	3854	3855
35	3040				3860	3841	3862	3863	3864	3865	3866	3867	3868	3869	3870	3871
2 2	2000				2874	3877	3878	3879	3880	3881	3882	3863	3884	3885	3886	3887
120	2000				3892	3893	3894	3895	38%	3897	3898	3866	3900	3901	3902	3903
2	2000					000	2010	100	0	0010	2017	2015	3916	3917	3918	3919
F40	3904				3408	525	01.0	1000	2912	200	1 000	2 6		0000	7000	2025
F50	3920				3924	3925	3926	392/	3928	3858	3930	383	3332	2000	1000	2000
EAO	3036				3940	3941	3942	3943	3944	3945	394	3947	3948	3949	3950	282
E 20	3952				3956	3957	3958	3959	3960	3961	3962	3963	3964	3962	3966	3967
2 6	3000				3077	3973	3974	3975	3976	3977	3978	3979	3980	3981	3982	3983
2 6	2000				3988	3989	3990	3991	3992	3993	3994	3995	3996	3997	3998	3999
	3004				4004	4005	4004	4007	4008	4004	4010	4011	4012	4013	4014	4015
, E	4016				4020	4021	4022	4023	4024	4025	4026	4027	4028	4029	4030	4031
3 5	200		7007	4035	407	4037	4038	4039	4040	4041	4042	4043	4044	4045	4046	4047
2.6	4032	•	100		4052	1053	4054	4055	40.56	4057	4058	4059	4060	4061	4062	4063
37.	5.5	4	200		404	25	4070	4071	4072	4073	4074	4075	4076	4077	4078	4079
25	4004	600	5000		1000	4085	408	4087	4088	4089	4090	4091	4092	4093	4094	4095
5	4000	4	4005		5	3	2									

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